

August 15, 2025  
Project No. 34397-25

2684742 Ontario Inc.

**Re: Servicing and Stormwater Management Report  
Proposed Semi Detached Dwellings  
271 and 281 Doyle Street, Township of Southgate**

## **1.0 Introduction**

Van Harten Surveying Inc. (Van Harten) was retained to prepare a Servicing and Stormwater Management Report in support of the severance application for proposed semi-detached dwellings at 271 and 281 Doyle Street, Dundalk.

The purpose of this Servicing and Stormwater Management Report is to outline proposed water servicing, sanitary servicing, and stormwater servicing for the proposed development.

## **2.0 Existing Site Conditions**

The existing property consists of two residential lots each with a residence, driveway, and ancillary structures. The site is generally vegetated with maintained domestic grass and encompasses an area of approximately 0.144 ha. The property is bounded by existing residential properties to the east and west, Artemesia Street to the north and Doyle Street to the south. Existing driveway access is from Doyle Street.

## **3.0 Proposed Development Conditions**

The proposed development will be comprised of six semi-detached units each with driveway access to Doyle Street.

## **4.0 Water Servicing**

### **4.1 Existing Water Servicing**

#271 Doyle Street is serviced by an existing drilled well near the front west corner of the building. No well was identified on the topographic survey for #281. Per record drawings, there are existing 150mm watermains on the south side of each Doyle Street and Artemesia Street. Record drawings illustrate water service connections for each #281 and #271 Doyle installed to the street line. The topographic survey located an existing curbstop for #281 and no curbstop was located for #271. It is unclear whether #271 was pre-serviced with a municipal water service connection.

There is an existing 150mmØ watermain along the north side of Eco Parkway. There are no water services to the site in the existing condition. There is an existing fire hydrant on the south side of Doyle opposite house #271.

## 4.2 Proposed Water Servicing

The water demand for the proposed development was completed with reference to the Township of Southgate Municipal Servicing Standards (June 2022) and the Ministry of Environment Design Guidelines for Drinking-Water Systems (2008). The water demand for the proposed development can be referenced in Table 1. Detailed water demand calculations have been provided in Attachment C. Referencing Table 1, the maximum daily water demand and the peak hour water demand for the proposed development are 0.89 L/s and 1.34 L/s, respectively.

*Table 1: Water Demand Calculations - Proposed Development*

| Design Guidelines | Average Daily Flow (L/s) | Max. Daily Flow (L/s) | Peak Hour Design Flow (L/s) |
|-------------------|--------------------------|-----------------------|-----------------------------|
| Southgate/MOE     | 0.09                     | 0.89                  | 1.34                        |

Each lot will be provided with a minimum 25mm water service connecting to the existing 150mm watermain on the south side of Doyle Street.

The existing fire hydrant will provide fire protection for the proposed development.

Details of the proposed water servicing can be referenced on the Site Servicing Plan (Drawing C02, as amended).

## 5.0 Sanitary Servicing

### 5.1 Existing Sanitary Servicing

With reference to the drawings for Project No. 14-262 (White Rose Park Subdivision, Township of Southgate), there is an existing 200mm diameter PVC sanitary on Artemesia Street and Doyle Street and each property (#271 and #281) have existing sanitary connections to the sewer on Doyle Street.

### 5.2 Proposed Sanitary Servicing

The sanitary demand for the proposed development was completed with reference to the Township of Southgate Municipal Servicing Standards (June 2022). The sanitary demand for the proposed development can be referenced in Table 2. Detailed sanitary demand calculations have

been provided in Attachment C. Referring to Table 2, the peak sanitary design flow for the development is 0.31 L/s.

*Table 2: Sanitary Demand Calculations – Proposed Development*

| Design Guidelines | Peak Residential Flow (L/s) | Peak Infiltration Flow (L/s) | Peak Design Flow (L/s) |
|-------------------|-----------------------------|------------------------------|------------------------|
| Southgate         | 0.29                        | 0.02                         | 0.31                   |

Each lot will be provided with a 100mm PVC SDR 28 sanitary sewer connecting to the existing 200mm diameter PVC sanitary sewer on Doyle Street.

## 6.0 Stormwater Management

### 6.1 Stormwater Management Criteria

The Township of Southgate Municipal Servicing Standards (June 2022) and the Ministry of Environment Stormwater Management Planning and Design Manual (March 2003) were referenced to determine the stormwater management criteria for the proposed development. Based on the manuals the following stormwater criteria must be met:

**Stormwater Quantity Control** – Control of post-development runoff flows to pre-development levels for rainfall events with return periods between the 5 year and 100 year storm event.

**Stormwater Quality Control** – Provide enhanced protection - 80% total suspended solid (TSS) removal.

### 6.2 Existing Drainage Patterns

An Existing Drainage Plan has been prepared based on the topographic survey. The site generally slopes from the southwest to the northeast with a total topographic relief of approximately 1.2m. The majority of stormwater from the property drains overland to Artemesia Street and the existing 300mm storm sewer on Artemesia.

Two (2) catchments were identified in the pre-development condition:

- Catchment 101 – Represents the drainage area that drains via sheet flow to Artemesia Street.
- Catchment 102 – Represents the drainage area directed to adjacent private property to the east (House #261).

Table 2 summarizes the pre-development drainage areas and hydrologic design parameters. The Pre-Development Drainage Plan can be referenced in the Appendix.

*Table 2: Pre-development Catchments and Hydrologic Design Parameters*

| <b>Hydrologic Parameter</b> | <b>Catchment 101</b> | <b>Catchment 102</b> |
|-----------------------------|----------------------|----------------------|
| Hydrograph                  | NasHyd               | NasHyd               |
| Catchment Area (ha)         | 0.132                | 0.012                |
| Curve Number                | CN = 76.59           | CN = 74.34           |
| Initial Abstraction (mm)    | 4.68                 | 4.96                 |
| Slope (%)                   | 2.9                  | 3.3                  |
| Time to Peak (hr)           | 0.12                 | 0.05                 |

### **6.3 Proposed Drainage Patterns**

A proposed drainage plan has been prepared based on the Site Grading Plan prepared by Van Harten. Under post-development conditions, three catchments were identified:

- Catchment 201 – Consists of the landscape rear and side yards and the building roofs draining to Artemesia Street.
- Catchment 202 – Consists of the building roofs which drain to an infiltration gallery with overflow to Artemesia Street.
- Catchment 203 – Consists of the driveway areas and front yards draining uncontrolled to Doyle Street.

Table 3 summarizes the post-development drainage areas and hydrologic design parameters. The Post-Development Drainage Plan can be referenced in the Appendix.

*Table 3: Post Development Catchments and Hydrologic Design Parameters*

| Hydrologic Parameter                          | Catchment 201 | Catchment 202 |     | Catchment 203 |     |
|-----------------------------------------------|---------------|---------------|-----|---------------|-----|
| Hydrograph                                    | NasHyd        | StanHyd       |     | StanHyd       |     |
| Catchment Area (ha)                           | 0.066         | 0.050         |     | 0.029         |     |
| Percent Imperv (%) / Curve Number             | CN=74         | 100%          |     | 56.9%         |     |
| Initial Abstraction   Depression Storage (mm) | 5.0           | 5.0           | 2.0 | 5.0           | 2.0 |
| Slope (%)<br>(Perv   Imperv)                  | 2.9           | 2.0           | 8.0 | 2.0           | 2.0 |
| Time to Peak (hr)                             | 0.13          | -             |     | -             |     |

#### 6.4 Stormwater Quantity Controls

The stormwater management quantity control criteria for the site are subject to the Township of Southgate Municipal Servicing Standards. The quantity control criterion for the proposed development includes controlling the post-development peak flows to the pre-development peak flow rates for the 5-year through 100-year storm events.

Calculations were prepared using Visual Otthymo and IDF parameters obtained from the MTO Lookup Tool – Dundalk Specific IDF to calculate the return period peak flows under the pre-development and post-development conditions for the 5-year through 100-year return periods (Tables 4, 5 and 6). The Visual Otthymo output files are provided in Appendix B.

*Table 4: Peak Flow and Storage Requirements Summary (Catchment 201 & 202) – Artemesia Street*

| Storm Event (yr) | Pre-Development Peak Flow (m <sup>3</sup> /s) | Post-Development Controlled Peak Flow (m <sup>3</sup> /s) | Required Storage (m <sup>3</sup> ) | Provided Storage (m <sup>3</sup> ) |
|------------------|-----------------------------------------------|-----------------------------------------------------------|------------------------------------|------------------------------------|
| 5                | 0.005                                         | 0.003                                                     | 19.2                               | 19.2                               |
| 10               | 0.007                                         | 0.004                                                     | 19.2                               |                                    |
| 25               | 0.010                                         | 0.006                                                     | 19.2                               |                                    |
| 50               | 0.013                                         | 0.011                                                     | 19.2                               |                                    |
| 100              | 0.015                                         | 0.015                                                     | 19.2                               |                                    |

<sup>1</sup> Pre-Development Peak Flows = Catchment 101

<sup>2</sup> Post-Development Controlled Peak Flow = Catchment 201 + Catchment 202

*Table 5: Peak Flow Summary (Doyle Street)*

| Storm Event (yr) | Catchment 203 Peak Flow (m <sup>3</sup> /s) | Increase (L/s) |
|------------------|---------------------------------------------|----------------|
| 5                | 0.009                                       | 9              |
| 10               | 0.011                                       | 11             |
| 25               | 0.013                                       | 13             |
| 50               | 0.015                                       | 15             |
| 100              | 0.017                                       | 17             |

*Table 6: Peak Flow Summary (Property)*

| Storm Event (yr) | Site (Pre-Dev) | Site (Post-Dev) | Increase (L/s) |
|------------------|----------------|-----------------|----------------|
| 5                | 0.006          | 0.011           | 5              |
| 10               | 0.008          | 0.014           | 6              |
| 25               | 0.011          | 0.017           | 6              |
| 50               | 0.014          | 0.020           | 6              |
| 100              | 0.016          | 0.023           | 7              |

<sup>1</sup> Pre-Development Peak Flows = Catchment 101 + 102

<sup>2</sup> Post-Development Controlled Peak Flow = Catchment 201 + 202 + 203

Quantity controls are required to attenuate the post-development peak flows to the pre-development levels. Quantity controls for the proposed development will be provided by routing the building roofs to sub-surface infiltration galleries (one per lot). Each gallery will provide a volume of 3.2 cu.m. with a combined volume across the property of 19.2 cu.m..

Building downspouts are to be routed to the subsurface gallery on each lot and be provided with overflow to grade and out to Artemesia Street.

Flows are projected to increase post-development from the property. This is as a result of the additional driveways to Doyle Street.

## **6.5 Stormwater Quality Controls**

It is our understanding that the water quality related criterion for this property is Enhanced (80% longterm TSS removal).

The proposal is an infill development consisting of six semi-detached lots and no new roadways are proposed. Considering the nature of the proposed development, all runoff generated by these properties, with the exception of driveway areas, can be considered “clean” and not subject to requirements for additional polishing. Together, the driveways cover an approximate area of 163 sq.m.. This area represents 11% of the total property area and an increase in driveway area of 106 sq.m. The driveway area represents a small portion of the overall development and will not have a significant impact on the downstream stormwater system.

The following are proposed to support water quality objectives for the property:

- To the extent possible, impervious areas are to be directed to grassed areas to encourage filtration and infiltration of runoff;
- Building downspouts are to be diverted to infiltration galleries in the rear yard of each lot;
- Where possible, grass swales should have a trapezoidal rather than triangular cross-section to reduce flow depths and velocities;
- The rear yards will be graded to reduce flow concentrations and encourage sheet flow along the rear lot line.

## **6.6 Operation and Maintenance**

The future property owners will be required to inspect the works on an annual basis to ensure their continued functioning.

- All downspouts, splash pads and roof leaders shall be kept in good working order at all times.
- For the roof leaders connected to the infiltration galleries, the debris screen should be periodically removed, cleaned of debris, inspected for integrity and reinstalled. We suggest that this should be undertaken at minimum in November and April of any given calendar year, or as needed to support their continued operation;
- Inspection ports are to be installed on the infiltration galleries for regular inspection and monitoring of rainwater drawdown times following major storm events;

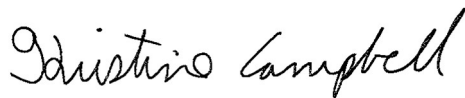
- All grass swales should be maintained free clear of obstructions so that they function as intended. The property owner should inspect on a routine basis for erosion, in particular at downspout locations, and repair any gullies, rills or bare spots;
- Should the drawdown of the soakaway exceed 72 hours following a major storm event, the clear stone reservoir should be replaced to restore function.

The maintenance of the stormwater management features on the site is the sole responsibility of each property owner and should be completed on an as needed basis.

## **7.0 Closure**

The completed Servicing and Stormwater Management Report is specific to the site based on our knowledge of the proposed development. We trust that this report is suitable to support the severance application for the proposed development. Please contact our office if you have any questions or require further consultation.

**VAN HARTEN SURVEYING INC.**



**Kristine Campbell, P. Eng.**



Encl. Attachment A – Figures

Encl. Attachment B - Stormwater Management Calculations

Enc. Attachment C – Sanitary and Water Demand Calculations



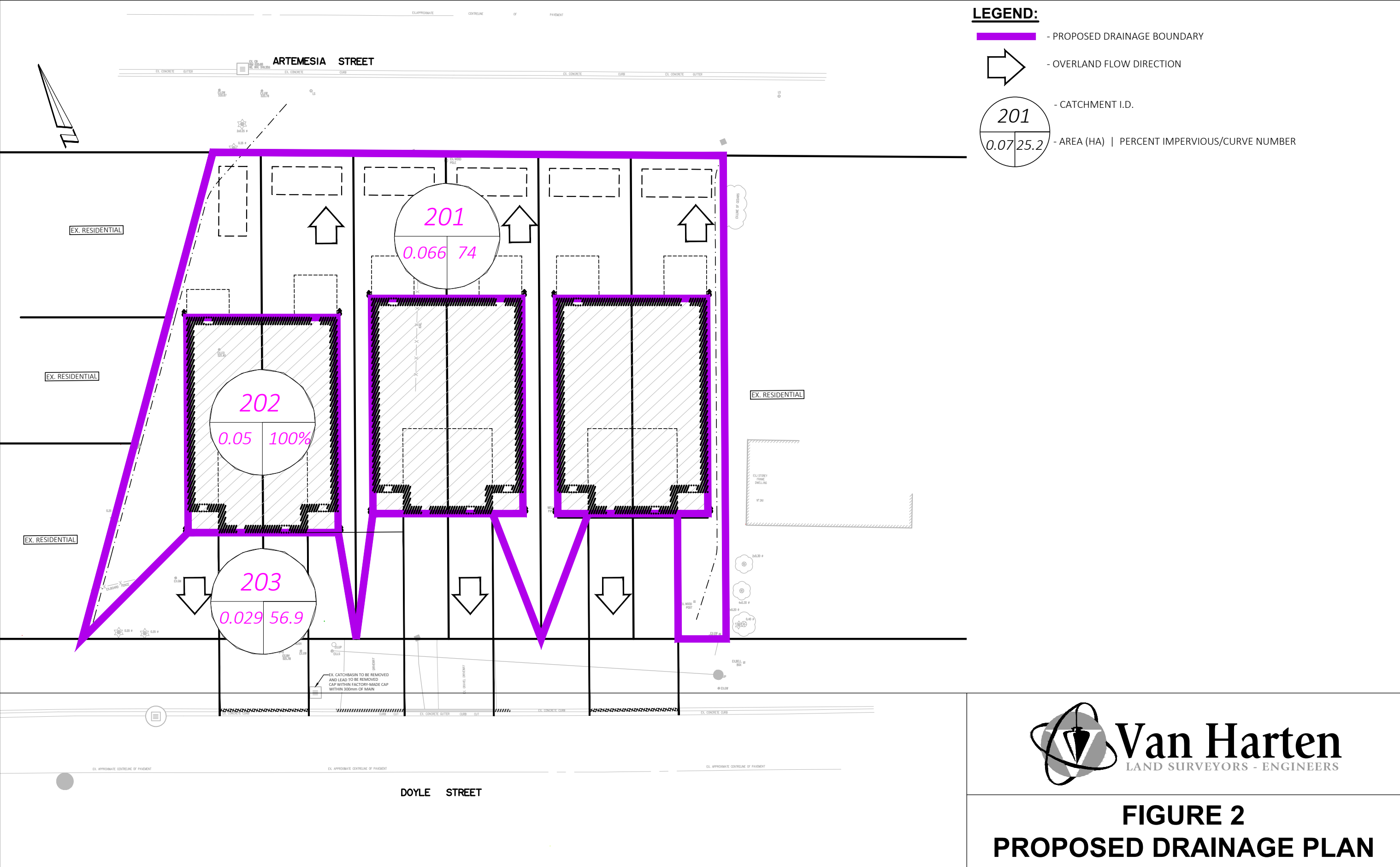
## **ATTACHMENT A**

### **FIGURES**

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- Figure 1 – Existing Conditions Drainage Plan
- Figure 2 – Proposed Conditions Drainage Plan





**FIGURE 2**  
**PROPOSED DRAINAGE PLAN**

## **ATTACHMENT B**

### **STORMWATER CALCULATIONS**

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- MTO Lookup Tool – IDF Parameters
- Table B.1a – Pre-Development Catchment 101 Parameters
- Table B.1b – Pre-Development Catchment 102 Parameters
- Table B.2a – Post-Development Catchment 201 Parameters
- Table B.2b – Post Development Catchment 202 Parameters
- Table B.2c – Post Development Catchment 203 Parameters
- VO Output

Active coordinate

44° 10' 15" N, 80° 23' 45" W (44.170833,-80.395833)

Retrieved: Thu, 14 Aug 2025 16:34:57 GMT



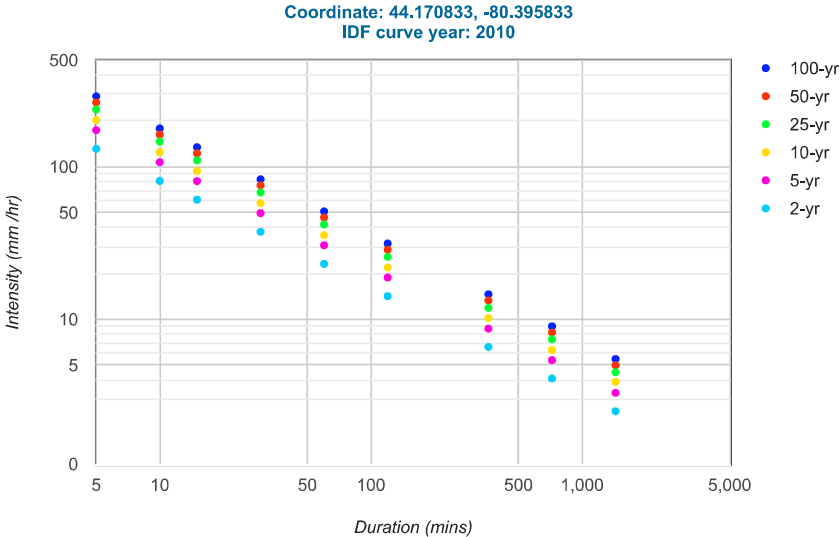
Location summary

These are the locations in the selection.

IDF Curve: 44° 10' 15" N, 80° 23' 45" W (44.170833,-80.395833)

Results

An IDF curve was found.



Coefficient summary

IDF Curve: 44° 10' 15" N, 80° 23' 45" W (44.170833,-80.395833)

Retrieved: Thu, 14 Aug 2025 16:34:57 GMT

Data year: 2010

IDF curve year: 2010

| Return period | 2-yr   | 5-yr   | 10-yr  | 25-yr  | 50-yr  | 100-yr |
|---------------|--------|--------|--------|--------|--------|--------|
| A             | 23.1   | 30.6   | 35.6   | 41.8   | 46.5   | 51.0   |
| B             | -0.699 | -0.699 | -0.699 | -0.699 | -0.699 | -0.699 |

Statistics

Rainfall intensity (mm hr<sup>-1</sup>)

| Duration | 5-min | 10-min | 15-min | 30-min | 1-hr | 2-hr | 6-hr | 12-hr | 24-hr |
|----------|-------|--------|--------|--------|------|------|------|-------|-------|
| 2-yr     | 131.2 | 80.8   | 60.9   | 37.5   | 23.1 | 14.2 | 6.6  | 4.1   | 2.5   |
| 5-yr     | 173.8 | 107.1  | 80.6   | 49.7   | 30.6 | 18.8 | 8.7  | 5.4   | 3.3   |
| 10-yr    | 202.2 | 124.6  | 93.8   | 57.8   | 35.6 | 21.9 | 10.2 | 6.3   | 3.9   |
| 25-yr    | 237.4 | 146.3  | 110.2  | 67.9   | 41.8 | 25.7 | 11.9 | 7.4   | 4.5   |
| 50-yr    | 264.1 | 162.7  | 122.5  | 75.5   | 46.5 | 28.6 | 13.3 | 8.2   | 5.0   |
| 100-yr   | 289.7 | 178.4  | 134.4  | 82.8   | 51.0 | 31.4 | 14.6 | 9.0   | 5.5   |

Rainfall depth (mm)

| Duration | 5-min | 10-min | 15-min | 30-min | 1-hr | 2-hr | 6-hr | 12-hr | 24-hr |
|----------|-------|--------|--------|--------|------|------|------|-------|-------|
| 2-yr     | 10.9  | 13.5   | 15.2   | 18.8   | 23.1 | 28.5 | 39.6 | 48.8  | 60.1  |
| 5-yr     | 14.5  | 17.8   | 20.2   | 24.8   | 30.6 | 37.7 | 52.5 | 64.6  | 79.6  |
| 10-yr    | 16.9  | 20.8   | 23.5   | 28.9   | 35.6 | 43.9 | 61.0 | 75.2  | 92.7  |
| 25-yr    | 19.8  | 24.4   | 27.5   | 33.9   | 41.8 | 51.5 | 71.7 | 88.3  | 108.8 |
| 50-yr    | 22.0  | 27.1   | 30.6   | 37.7   | 46.5 | 57.3 | 79.7 | 98.2  | 121.0 |
| 100-yr   | 24.1  | 29.7   | 33.6   | 41.4   | 51.0 | 62.8 | 87.5 | 107.7 | 132.7 |

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Project No: 34397-25  
 Project Name: Proposed Semi Detached Dwellings  
 Project Location: 271 Doyle Street, Southgate  
 Date: 8/15/2025  
 Update: 8/15/2025



## Table B.1a Pre-Development Catchment 101 NASHYD Hydraulic Parameter Sheet

Catchment Area: 0.132 ha

### On-site Soils:

| Type               | Classification |
|--------------------|----------------|
| Listowel silt loam |                |

### Impervious Land Use:

| Roadway/Driveway |    | Gravel |    | Building |    | SWM Facility |    | Total |             |
|------------------|----|--------|----|----------|----|--------------|----|-------|-------------|
| Area             | CN | Area   | CN | Area     | CN | Area         | CN | Area  | Weighted CN |
| 0.004            | 98 |        |    | 0.011    | 98 |              |    | 0.014 | 98.00       |

\*All areas are in Hectares.

### Pervious Land Use:

| Lawn  |    | Woodland |    | Field |    | Wetland |    | Total |             |
|-------|----|----------|----|-------|----|---------|----|-------|-------------|
| Area  | CN | Area     | CN | Area  | CN | Area    | CN | Area  | Weighted CN |
| 0.117 | 74 |          |    |       |    |         |    | 0.117 | 74.00       |

\*All areas are in Hectares.

### Composite Initial Abstraction:

| Landuse            | IA (mm) | Area  |
|--------------------|---------|-------|
| Lawn               | 5       | 0.117 |
| Woodland           | 10      | 0.000 |
| Cultivated         | 7       | 0.000 |
| Wetland            | 16      | 0.000 |
| Impervious         | 2       | 0.014 |
| Catchment Weighted | 4.68    | 0.132 |

### Composite Runoff Coefficient:

| Landuse            | RC   | Area  |
|--------------------|------|-------|
| Lawn               | 0.25 | 0.117 |
| Woodland           |      | 0.000 |
| Cultivated         |      | 0.000 |
| Wetland            |      | 0.000 |
| Impervious         | 0.9  | 0.014 |
| Catchment Weighted | 0.32 | 0.132 |

Composite Curve Number: 76.59  
 Composite Initial Abstraction (mm): 4.68  
 Composite Runoff Coefficient: 0.32  
 Flow Length (m): 34  
 Slope (%): 2.9  
 Time to Concentration (hr) - Airport Method: 0.17  
 Time to Peak (hr): 0.12

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## Table B.1b Pre-Development Catchment 102 NASHYD Hydraulic Parameter Sheet

Catchment Area: 0.012 ha

### On-site Soils:

| Type               | Classification |
|--------------------|----------------|
| Listowel silt loam |                |

### Impervious Land Use:

| Roadway/Driveway |    | Gravel |    | Building |    | SWM Facility |    | Total |             |
|------------------|----|--------|----|----------|----|--------------|----|-------|-------------|
| Area             | CN | Area   | CN | Area     | CN | Area         | CN | Area  | Weighted CN |
| 0.000            | 98 |        |    |          |    |              |    | 0.000 | 98.00       |

\*All areas are in Hectares.

### Pervious Land Use:

| Lawn  |    | Woodland |    | Field |    | Wetland |    | Total |             |
|-------|----|----------|----|-------|----|---------|----|-------|-------------|
| Area  | CN | Area     | CN | Area  | CN | Area    | CN | Area  | Weighted CN |
| 0.012 | 74 |          |    |       |    |         |    | 0.012 | 74.00       |

\*All areas are in Hectares.

### Composite Initial Abstraction:

| Landuse            | IA (mm) | Area  |
|--------------------|---------|-------|
| Lawn               | 5       | 0.012 |
| Woodland           | 10      | 0.000 |
| Cultivated         | 7       | 0.000 |
| Wetland            | 16      | 0.000 |
| Impervious         | 2       | 0.000 |
| Catchment Weighted | 4.96    | 0.012 |

### Composite Runoff Coefficient:

| Landuse            | RC   | Area  |
|--------------------|------|-------|
| Lawn               | 0.25 | 0.012 |
| Woodland           |      | 0.000 |
| Cultivated         |      | 0.000 |
| Wetland            |      | 0.000 |
| Impervious         | 0.9  | 0.000 |
| Catchment Weighted | 0.26 | 0.012 |

Composite Curve Number: 74.34  
 Composite Initial Abstraction (mm): 4.96  
 Composite Runoff Coefficient: 0.26  
 Flow Length (m): 6  
 Slope (%): 3.3  
 Time to Concentration (hr) - Airport Method: 0.08  
 Time to Peak (hr): 0.05



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## Table B.2a Post-Development Catchment 201 NASHYD Hydraulic Parameter Sheet

Catchment Area: 0.066 ha

### On-site Soils:

| Type               | Classification |
|--------------------|----------------|
| Listowel silt loam |                |

### Impervious Land Use:

| Roadway/Driveway |    | Gravel |    | Building |    | SWM Facility |    | Total |             |
|------------------|----|--------|----|----------|----|--------------|----|-------|-------------|
| Area             | CN | Area   | CN | Area     | CN | Area         | CN | Area  | Weighted CN |
|                  |    |        |    |          |    |              |    |       |             |

\*All areas are in Hectares.

### Pervious Land Use:

| Lawn  |    | Woodland |    | Field |    | Wetland |    | Total |             |
|-------|----|----------|----|-------|----|---------|----|-------|-------------|
| Area  | CN | Area     | CN | Area  | CN | Area    | CN | Area  | Weighted CN |
| 0.066 | 74 |          |    |       |    |         |    | 0.066 | 74.00       |

\*All areas are in Hectares.

### Composite Initial Abstraction:

| Landuse            | IA (mm) | Area  |
|--------------------|---------|-------|
| Lawn               | 5       | 0.066 |
| Woodland           | 10      | 0.000 |
| Cultivated         | 7       | 0.000 |
| Wetland            | 16      | 0.000 |
| Impervious         | 2       | 0.000 |
| Catchment Weighted | 5.00    | 0.066 |

### Composite Runoff Coefficient:

| Landuse            | RC   | Area  |
|--------------------|------|-------|
| Lawn               | 0.25 | 0.066 |
| Woodland           |      | 0.000 |
| Cultivated         |      | 0.000 |
| Wetland            |      | 0.000 |
| Impervious         | 0.9  | 0.000 |
| Catchment Weighted | 0.25 | 0.066 |

Composite Curve Number: 74.00  
 Composite Initial Abstraction (mm): 5.00  
 Composite Runoff Coefficient: 0.25  
 Flow Length (m): 34  
 Slope (%): 2.9  
 Time to Concentration (hr) - Airport Method: 0.19  
 Time to Peak (hr): 0.13

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## Table B.2b Post-Development Catchment 202 STANHYD Hydraulic Parameter Sheet

Catchment Area: 0.050

### On-site Soils:

| Type               | Classification |
|--------------------|----------------|
| Listowel silt loam |                |

### Impervious Land Use:

| Roadway/Driveway |    | Gravel |    | Building |    | SWM Facility |    | Total |             |
|------------------|----|--------|----|----------|----|--------------|----|-------|-------------|
| Area             | CN | Area   | CN | Area     | CN | Area         | CN | Area  | Weighted CN |
|                  |    |        |    | 0.050    | 98 |              |    | 0.050 | 98.00       |

\*All areas are in Hectares.

### Impervious Land Use VO Inputs:

Depression Storage (mm): 1  
 Slope (%): 8  
 Flow Length (m from model): 18.26  
 Total Indirectly Connected Impervious Area (ha): 0.050  
 Total Directly Connected Impervious Area (ha): 0.050  
 T IMP: 0.999 <<< <1 for computation purposes  
 X IMP: 0.999 <<< <1 for computation purposes

### Pervious Land Use:

| Lawn |    | Woodland |    | Cultivated |    | Wetland |    | Total |             |
|------|----|----------|----|------------|----|---------|----|-------|-------------|
| Area | CN | Area     | CN | Area       | CN | Area    | CN | Area  | Weighted CN |
|      |    |          |    |            |    |         |    |       |             |

\*All areas are in Hectares.

### Pervious Land Use VO Inputs:

Pervious Curve Number: 0.0  
 Initial Abstraction (mm): 5.00  
 Slope (%): 2  
 Flow Length (m): 13  
 RC 0.90

### Pervious Initial Abstraction:

| Landuse            | IA (mm) | Area  |
|--------------------|---------|-------|
| Lawn               | 5       | 0.000 |
| Woodland           | 10      | 0     |
| Cultivated         | 7       | 0     |
| Wetland            | 16      | 0     |
| Catchment Weighted | #DIV/0! | 0     |

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## Table B.2c Post-Development Catchment 203 STANHYD Hydraulic Parameter Sheet

Catchment Area: 0.029

### On-site Soils:

| Type               | Classification |
|--------------------|----------------|
| Listowel silt loam |                |

### Impervious Land Use:

| Roadway/Driveway |    | Gravel |    | Building |    | SWM Facility |    | Total |             |
|------------------|----|--------|----|----------|----|--------------|----|-------|-------------|
| Area             | CN | Area   | CN | Area     | CN | Area         | CN | Area  | Weighted CN |
| 0.016            | 98 |        |    |          |    |              |    | 0.016 | 98.00       |

\*All areas are in Hectares.

### Impervious Land Use VO Inputs:

Depression Storage (mm): 2  
Slope (%): 2  
Flow Length (m from model): 13.9  
Total Indirectly Connected Impervious Area (ha): 0.016  
Total Directly Connected Impervious Area (ha): 0.016  
T IMP: 0.569  
X IMP: 0.569

### Pervious Land Use:

| Lawn  |    | Woodland |    | Cultivated |    | Wetland |    | Total     |             |
|-------|----|----------|----|------------|----|---------|----|-----------|-------------|
| Area  | CN | Area     | CN | Area       | CN | Area    | CN | Area      | Weighted CN |
| 0.012 | 74 |          |    |            |    |         |    | 0.0123714 | 74.00       |

\*All areas are in Hectares.

### Pervious Land Use VO Inputs:

Pervious Curve Number: 74.0  
Initial Abstraction (mm): 5.00  
Slope (%): 2  
Flow Length (m): 9  
RC 0.51

### Pervious Initial Abstraction:

| Landuse            | IA (mm) | Area      |
|--------------------|---------|-----------|
| Lawn               | 5       | 0.012     |
| Woodland           | 10      | 0         |
| Cultivated         | 7       | 0         |
| Wetland            | 16      | 0         |
| Catchment Weighted | 5.00    | 0.0123714 |

```
=====
=====
```

```

      V      V      I      SSSSS  U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V      V      I      SS      U      U      AAAAA  L
      V      V      I      SS      U      U      A      A  L
      VV      I      SSSSS  UUUUU  A      A  LLLLL

```

```

      OOO      TTTTT  TTTTT  H      H      Y      Y  M      M      OOO      TM
      O      O      T      T      H      H      Y Y      MM MM  O      O
      O      O      T      T      H      H      Y      M      M  O      O
      OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

```

Input   filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2
\voindat
Output  filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\c2f1dec4-0813-4076-a76e-de6bb76
Summary filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\c2f1dec4-0813-4076-a76e-de6bb76

```

DATE: 08/14/2025

TIME: 02:48:40

USER:

COMMENTS:

```
-----
-----
```

```

*****
** SIMULATION : 100yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      |      IDF curve parameters: A= 892.273
| Ptotal= 70.98 mm  |                      B=   0.000
-----                      C=   0.699

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN  | TIME | RAIN   | TIME | RAIN  |
|------|-------|------|-------|------|--------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr |
| 0.00 | 7.65  | 0.75 | 26.87 | 1.50 | 16.60  |      |       |
| 2.25 | 9.39  | 0.08 | 8.18  | 0.83 | 49.98  | 1.58 | 15.15 |
| 2.33 | 9.01  | 0.17 | 8.82  | 0.92 | 289.68 | 1.67 | 13.97 |
| 2.42 | 8.66  | 0.25 | 9.60  | 1.00 | 61.34  | 1.75 | 12.99 |
| 2.50 | 8.34  | 0.33 | 10.56 | 1.08 | 38.68  | 1.83 | 12.17 |
| 2.58 | 8.05  | 0.42 | 11.80 | 1.17 | 29.50  | 1.92 | 11.46 |
| 2.67 | 7.78  | 0.50 | 13.47 | 1.25 | 24.30  | 2.00 | 10.84 |
| 2.75 | 7.53  | 0.58 | 15.86 | 1.33 | 20.88  | 2.08 | 10.30 |
| 2.83 | 7.30  | 0.67 | 19.65 | 1.42 | 18.44  | 2.17 | 9.82  |
| 2.92 | 7.09  |      |       |      |        |      |       |

```

-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 0.01 Curve Number
(CN)= 74.3
|ID= 1 DT=10.0 min | Ia (mm)= 4.96 # of Linear
Res. (N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

| ---- TRANSFORMED HYETOGRAPH ---- |       |       |        |       |       |       |       |
|----------------------------------|-------|-------|--------|-------|-------|-------|-------|
| TIME                             | RAIN  | TIME  | RAIN   | TIME  | RAIN  | TIME  | RAIN  |
| hrs                              | mm/hr | hrs   | mm/hr  | hrs   | mm/hr | hrs   | mm/hr |
| 0.167                            | 7.92  | 1.000 | 169.83 | 1.833 | 13.48 |       |       |
| 2.67                             | 8.19  | 0.333 | 9.21   | 1.167 | 50.01 | 2.000 | 11.81 |
| 2.83                             | 7.66  |       |        |       |       |       |       |

|      |      |       |       |  |       |       |  |       |       |  |
|------|------|-------|-------|--|-------|-------|--|-------|-------|--|
| 3.00 | 7.20 | 0.500 | 11.18 |  | 1.333 | 26.90 |  | 2.167 | 10.57 |  |
|      |      | 0.667 | 14.66 |  | 1.500 | 19.66 |  | 2.333 | 9.61  |  |
|      |      | 0.833 | 23.26 |  | 1.667 | 15.87 |  | 2.500 | 8.83  |  |

Unit Hyd Qpeak (cms)= 0.003

PEAK FLOW (cms)= 0.001 (i)  
 TIME TO PEAK (hrs)= 1.167  
 RUNOFF VOLUME (mm)= 26.987  
 TOTAL RAINFALL (mm)= 70.976  
 RUNOFF COEFFICIENT = 0.380

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 0.13 Curve Number
(CN)= 76.5
| ID= 1 DT=10.0 min | Ia (mm)= 4.68 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.12

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

|      |       | ---- TRANSFORMED HYETOGRAPH ---- |       |  |       |        |  |       |       |
|------|-------|----------------------------------|-------|--|-------|--------|--|-------|-------|
| TIME | RAIN  | TIME                             | RAIN  |  | TIME  | RAIN   |  | TIME  | RAIN  |
| hrs  | mm/hr | hrs                              | mm/hr |  | hrs   | mm/hr  |  | hrs   | mm/hr |
| 2.67 | 8.19  | 0.167                            | 7.92  |  | 1.000 | 169.83 |  | 1.833 | 13.48 |
| 2.83 | 7.66  | 0.333                            | 9.21  |  | 1.167 | 50.01  |  | 2.000 | 11.81 |
| 3.00 | 7.20  | 0.500                            | 11.18 |  | 1.333 | 26.90  |  | 2.167 | 10.57 |
|      |       | 0.667                            | 14.66 |  | 1.500 | 19.66  |  | 2.333 | 9.61  |
|      |       | 0.833                            | 23.26 |  | 1.667 | 15.87  |  | 2.500 | 8.83  |

Unit Hyd Qpeak (cms)= 0.042

PEAK FLOW (cms)= 0.015 (i)  
 TIME TO PEAK (hrs)= 1.000  
 RUNOFF VOLUME (mm)= 26.129  
 TOTAL RAINFALL (mm)= 70.976  
 RUNOFF COEFFICIENT = 0.368

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

-----

| ADD HYD ( 0007)   |  | AREA | QPEAK | TPEAK | R.V.  |
|-------------------|--|------|-------|-------|-------|
| 1 + 2 = 3         |  | (ha) | (cms) | (hrs) | (mm)  |
| ID1= 1 ( 0101):   |  | 0.13 | 0.015 | 1.00  | 26.13 |
| + ID2= 2 ( 0102): |  | 0.01 | 0.001 | 1.17  | 26.99 |
| =====             |  |      |       |       |       |
| ID = 3 ( 0007):   |  | 0.14 | 0.016 | 1.00  | 26.20 |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

=====

```

      V      V      I      SSSSS  U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V V      I      SS      U      U      AAAAA L
      V V      I      SS      U      U      A      A L
      VV      I      SSSSS  UUUUU  A      A  LLLLL

      OOO      TTTTT  TTTTT  H      H      Y      Y      M      M      OOO      TM
      O      O      T      T      H      H      Y Y      MM MM  O      O
      O      O      T      T      H      H      Y      M      M      O      O
      OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2  
 \voin.dat

Output filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\045c0475-  
 deb1-421f-9f8e-d461d7d

Summary filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\045c0475-  
 deb1-421f-9f8e-d461d7d

DATE: 08/14/2025

TIME: 02:48:40

USER:

COMMENTS:

```

-----
*****
** SIMULATION : 10yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      | IDF curve parameters: A= 622.842
| Ptotal= 49.54 mm |      B= 0.000
|                   |      C= 0.699
-----
                        used in:  INTENSITY = A / (t + B)^C

                        Duration of storm = 3.00 hrs
                        Storm time step   = 5.00 min
                        Time to peak ratio = 0.33

TIME      RAIN      TIME      RAIN | TIME      RAIN | TIME      RAIN |
hrs      mm/hr      hrs      mm/hr | hrs      mm/hr | hrs      mm/hr |
-----
0.00      5.34 | 0.75      18.76 | 1.50      11.59 |
2.25      6.56 | 0.08      5.71 | 1.58      10.57 |
2.33      6.29 | 0.17      6.16 | 1.67      9.75 |
2.42      6.04 | 0.25      6.70 | 1.75      9.07 |
2.50      5.82 | 0.33      7.37 | 1.83      8.49 |
2.58      5.62 | 0.42      8.24 | 1.92      8.00 |
2.67      5.43 | 0.50      9.40 | 2.00      7.57 |
2.75      5.26 | 0.58     11.07 | 2.08      7.19 |
2.83      5.10 | 0.67     13.71 | 2.17      6.86 |
2.92      4.95 |

```

```

-----
-----
| CALIB              |
| NASHYD ( 0102) | Area      (ha)= 0.01 Curve Number
(CN)= 74.3
| ID= 1 DT=10.0 min | Ia      (mm)= 4.96 # of Linear

```



Res. (N)= 3.00

----- U.H. Tp(hrs)= 0.17

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

```

              ----- TRANSFORMED HYETOGRAPH -----
TIME      RAIN      TIME      RAIN | TIME      RAIN | TIME      RAIN |
hrs      mm/hr      hrs      mm/hr | hrs      mm/hr | hrs      mm/hr |
2.67      5.72      0.167      5.53 | 1.000     118.55 | 1.833      9.41 |
2.83      5.34      0.333      6.43 | 1.167      34.91 | 2.000      8.25 |
3.00      5.02      0.500      7.81 | 1.333      18.77 | 2.167      7.38 |
              0.667     10.24 | 1.500      13.73 | 2.333      6.71 |
              0.833     16.24 | 1.667      11.08 | 2.500      6.17 |

```

Unit Hyd Qpeak (cms)= 0.003

PEAK FLOW (cms)= 0.001 (i)

TIME TO PEAK (hrs)= 1.167

RUNOFF VOLUME (mm)= 14.302

TOTAL RAINFALL (mm)= 49.544

RUNOFF COEFFICIENT = 0.289

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
-----

```

| CALIB |
| NASHYD ( 0101) | Area (ha)= 0.13 Curve Number
(CN)= 76.5
| ID= 1 DT=10.0 min | Ia (mm)= 4.68 # of Linear
Res. (N)= 3.00
----- U.H. Tp(hrs)= 0.12

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

```

              ----- TRANSFORMED HYETOGRAPH -----
TIME      RAIN      TIME      RAIN | TIME      RAIN | TIME      RAIN |
hrs      mm/hr      hrs      mm/hr | hrs      mm/hr | hrs      mm/hr |
2.67      5.72      0.167      5.53 | 1.000     118.55 | 1.833      9.41 |
2.83      5.34      0.333      6.43 | 1.167      34.91 | 2.000      8.25 |

```

```

3.00      5.02      0.500      7.81 | 1.333      18.77 | 2.167      7.38 |
              0.667      10.24 | 1.500      13.73 | 2.333      6.71 |
              0.833      16.24 | 1.667      11.08 | 2.500      6.17 |

```

Unit Hyd Qpeak (cms)= 0.042

PEAK FLOW (cms)= 0.007 (i)  
 TIME TO PEAK (hrs)= 1.000  
 RUNOFF VOLUME (mm)= 14.053  
 TOTAL RAINFALL (mm)= 49.544  
 RUNOFF COEFFICIENT = 0.284

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

```

-----
| ADD HYD ( 0007) |
| 1 + 2 = 3 |
-----
              AREA      QPEAK      TPEAK      R.V.
              (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0101): 0.13    0.007      1.00      14.05
+ ID2= 2 ( 0102): 0.01    0.001      1.17      14.30
=====
ID = 3 ( 0007): 0.14    0.008      1.00      14.07

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----  
 =====  
 =====

```

      V      V      I      SSSSS      U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V V      I      SS      U      U      AAAAA      L
      V V      I      SS      U      U      A      A      L
      VV      I      SSSSS      UUUUU      A      A      LLLLL
      OOO      TTTTT      TTTTT      H      H      Y      Y      M      M      OOO      TM
      O      O      T      T      H      H      Y Y      MM MM      O      O
      O      O      T      T      H      H      Y      M      M      O      O
      OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2  
 \voin.dat  
 Output filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\8d0ea48a-  
 e90c-4bde-b58b-feb5ee2  
 Summary filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\8d0ea48a-  
 e90c-4bde-b58b-feb5ee2

DATE: 08/14/2025

TIME: 02:48:40

USER:

COMMENTS:

-----  
 -----  
 \*\*\*\*\*  
 \*\* SIMULATION : 25yr 3hr 5min Chicago \*\*  
 \*\*\*\*\*

-----  
 | CHICAGO STORM | IDF curve parameters: A= 731.314  
 | Ptotal= 58.17 mm | B= 0.000  
 ----- C= 0.699  
 used in: INTENSITY = A / (t + B)^C  
 Duration of storm = 3.00 hrs  
 Storm time step = 5.00 min  
 Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN   | TIME | RAIN  | TIME | RAIN  |
|------|-------|------|--------|------|-------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr | hrs  | mm/hr |
| 0.00 | 6.27  | 0.75 | 22.03  | 1.50 | 13.60 |      |       |
| 2.25 | 7.70  | 0.83 | 40.97  | 1.58 | 12.41 |      |       |
| 2.33 | 7.38  | 0.92 | 237.42 | 1.67 | 11.45 |      |       |
| 2.42 | 7.10  | 1.00 | 50.28  | 1.75 | 10.65 |      |       |
| 2.50 | 6.83  | 1.08 | 31.70  | 1.83 | 9.97  |      |       |
| 2.58 | 6.60  | 1.17 | 24.17  | 1.92 | 9.39  |      |       |
| 2.67 | 6.38  |      |        |      |       |      |       |

|      |      |      |       |  |      |       |  |      |      |  |
|------|------|------|-------|--|------|-------|--|------|------|--|
| 2.75 | 6.17 | 0.50 | 11.04 |  | 1.25 | 19.91 |  | 2.00 | 8.89 |  |
| 2.83 | 5.99 | 0.58 | 13.00 |  | 1.33 | 17.12 |  | 2.08 | 8.44 |  |
| 2.92 | 5.81 | 0.67 | 16.10 |  | 1.42 | 15.12 |  | 2.17 | 8.05 |  |

```

-----
-----
-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 0.01 Curve Number
(CN)= 74.3
| ID= 1 DT=10.0 min | Ia (mm)= 4.96 # of Linear
Res. (N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME      RAIN      TIME      RAIN | TIME      RAIN | TIME      RAIN |
hrs      mm/hr     hrs      mm/hr | hrs      mm/hr | hrs      mm/hr |
2.67      6.72      0.167    6.49 | 1.000   139.20 | 1.833    11.05 |
2.83      6.27      0.333    7.55 | 1.167    40.99 | 2.000     9.68 |
3.00      5.90      0.500    9.16 | 1.333    22.04 | 2.167     8.67 |
           0.667   12.02 | 1.500    16.12 | 2.333     7.87 |
           0.833   19.06 | 1.667    13.01 | 2.500     7.24 |

```

```

Unit Hyd Qpeak (cms)= 0.003
PEAK FLOW (cms)= 0.001 (i)
TIME TO PEAK (hrs)= 1.167
RUNOFF VOLUME (mm)= 19.126
TOTAL RAINFALL (mm)= 58.173
RUNOFF COEFFICIENT = 0.329

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 0.13 Curve Number
(CN)= 76.5
| ID= 1 DT=10.0 min | Ia (mm)= 4.68 # of Linear

```

Res. (N)= 3.00

----- U.H. Tp(hrs)= 0.12

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

```

              ----- TRANSFORMED HYETOGRAPH -----
TIME      RAIN      TIME      RAIN |  TIME      RAIN |  TIME      RAIN |
hrs      mm/hr      hrs      mm/hr |  hrs      mm/hr |  hrs      mm/hr |
2.67      6.72      0.167      6.49 |  1.000     139.20 |  1.833     11.05 |
2.83      6.27      0.333      7.55 |  1.167      40.99 |  2.000      9.68 |
3.00      5.90      0.500      9.16 |  1.333      22.04 |  2.167      8.67 |
              0.667     12.02 |  1.500      16.12 |  2.333      7.87 |
              0.833     19.06 |  1.667      13.01 |  2.500      7.24 |

```

Unit Hyd Qpeak (cms)= 0.042

PEAK FLOW (cms)= 0.010 (i)

TIME TO PEAK (hrs)= 1.000

RUNOFF VOLUME (mm)= 18.667

TOTAL RAINFALL (mm)= 58.173

RUNOFF COEFFICIENT = 0.321

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
-----

```

-----
| ADD HYD ( 0007) |
| 1 + 2 = 3 |
-----
          AREA      QPEAK      TPEAK      R.V.
          (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0101):    0.13    0.010      1.00    18.67
+ ID2= 2 ( 0102):    0.01    0.001      1.17    19.13
=====
ID = 3 ( 0007):    0.14    0.011      1.00    18.71

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
-----  
=====

```

      V      V      I      SSSSS      U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V      V      I      SS      U      U      AAAAA      L

```

```

V  V      I      SS      U      U      A      A      L
VV      I      SSSSS  UUUUU  A      A      LLLLL

```

```

    OOO      TTTTT  TTTTT  H      H      Y      Y      M      M      OOO      TM
O      O      T      T      H      H      Y      Y      MM      MM      O      O
O      O      T      T      H      H      Y      M      M      O      O
    OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

```

Input   filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2
\voim.dat
Output  filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\2d41c165-0d29-4ac5-b0b3-78efcfd
Summary filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\2d41c165-0d29-4ac5-b0b3-78efcfd

```

DATE: 08/14/2025

TIME: 02:48:40

USER:

COMMENTS:

-----

```

*****
** SIMULATION : 50yr 3hr 5min Chicago      **
*****

```

```

-----
| CHICAGO STORM      |
| Ptotal= 64.71 mm  |
-----

```

```

IDF curve parameters: A= 813.543
                      B=   0.000
                      C=   0.699

```

used in: INTENSITY =  $A / (t + B)^C$

```

Duration of storm = 3.00 hrs
Storm time step   = 5.00 min
Time to peak ratio = 0.33

```

```

TIME      RAIN | TIME      RAIN | ' TIME      RAIN |

```

| TIME | RAIN  | hrs  | mm/hr |  | hrs  | mm/hr  |  | hrs  | mm/hr |  |
|------|-------|------|-------|--|------|--------|--|------|-------|--|
| hrs  | mm/hr |      |       |  |      |        |  |      |       |  |
|      |       | 0.00 | 6.97  |  | 0.75 | 24.50  |  | 1.50 | 15.13 |  |
| 2.25 | 8.56  | 0.08 | 7.46  |  | 0.83 | 45.57  |  | 1.58 | 13.81 |  |
| 2.33 | 8.21  | 0.17 | 8.04  |  | 0.92 | 264.12 |  | 1.67 | 12.74 |  |
| 2.42 | 7.89  | 0.25 | 8.75  |  | 1.00 | 55.93  |  | 1.75 | 11.85 |  |
| 2.50 | 7.60  | 0.33 | 9.63  |  | 1.08 | 35.26  |  | 1.83 | 11.09 |  |
| 2.58 | 7.34  | 0.42 | 10.76 |  | 1.17 | 26.89  |  | 1.92 | 10.45 |  |
| 2.67 | 7.09  | 0.50 | 12.28 |  | 1.25 | 22.15  |  | 2.00 | 9.89  |  |
| 2.75 | 6.87  | 0.58 | 14.46 |  | 1.33 | 19.04  |  | 2.08 | 9.39  |  |
| 2.83 | 6.66  | 0.67 | 17.91 |  | 1.42 | 16.82  |  | 2.17 | 8.96  |  |
| 2.92 | 6.47  |      |       |  |      |        |  |      |       |  |

```

-----
-----
-----
| CALIB |
| NASHYD ( 0102) | Area (ha)= 0.01 Curve Number
(CN)= 74.3
|ID= 1 DT=10.0 min | Ia (mm)= 4.96 # of Linear
Res. (N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

|      |       | ---- TRANSFORMED HYETOGRAPH ---- |       |  |       |        |  |       |       |  |
|------|-------|----------------------------------|-------|--|-------|--------|--|-------|-------|--|
| TIME | RAIN  | TIME                             | RAIN  |  | TIME  | RAIN   |  | TIME  | RAIN  |  |
| hrs  | mm/hr | hrs                              | mm/hr |  | hrs   | mm/hr  |  | hrs   | mm/hr |  |
|      |       | 0.167                            | 7.22  |  | 1.000 | 154.85 |  | 1.833 | 12.29 |  |
| 2.67 | 7.47  | 0.333                            | 8.40  |  | 1.167 | 45.60  |  | 2.000 | 10.77 |  |
| 2.83 | 6.98  | 0.500                            | 10.20 |  | 1.333 | 24.52  |  | 2.167 | 9.64  |  |
| 3.00 | 6.56  | 0.667                            | 13.37 |  | 1.500 | 17.93  |  | 2.333 | 8.76  |  |
|      |       | 0.833                            | 21.21 |  | 1.667 | 14.47  |  | 2.500 | 8.05  |  |

Unit Hyd Qpeak (cms)= 0.003

PEAK FLOW (cms)= 0.001 (i)  
 TIME TO PEAK (hrs)= 1.167  
 RUNOFF VOLUME (mm)= 23.048  
 TOTAL RAINFALL (mm)= 64.714  
 RUNOFF COEFFICIENT = 0.356

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 0.13 Curve Number
(CN)= 76.5
| ID= 1 DT=10.0 min | Ia (mm)= 4.68 # of Linear
Res.(N)= 3.00
----- U.H. Tp(hrs)= 0.12
  
```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

```

----- TRANSFORMED HYETOGRAPH -----
TIME      RAIN      TIME      RAIN | TIME      RAIN | TIME      RAIN |
hrs      mm/hr      hrs      mm/hr | hrs      mm/hr | hrs      mm/hr |
2.67      7.47      0.167      7.22 | 1.000     154.85 | 1.833     12.29 |
2.83      6.98      0.333      8.40 | 1.167      45.60 | 2.000     10.77 |
3.00      6.56      0.500     10.20 | 1.333      24.52 | 2.167      9.64 |
              0.667     13.37 | 1.500      17.93 | 2.333      8.76 |
              0.833     21.21 | 1.667      14.47 | 2.500      8.05 |
  
```

Unit Hyd Qpeak (cms)= 0.042

PEAK FLOW (cms)= 0.013 (i)  
 TIME TO PEAK (hrs)= 1.000  
 RUNOFF VOLUME (mm)= 22.398  
 TOTAL RAINFALL (mm)= 64.714  
 RUNOFF COEFFICIENT = 0.346

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
| ADD HYD ( 0007) |
| 1 + 2 = 3 |
-----
AREA      QPEAK      TPEAK      R.V.
(ha)      (cms)      (hrs)      (mm)
  
```



|                   |      |       |      |       |
|-------------------|------|-------|------|-------|
| ID1= 1 ( 0101):   | 0.13 | 0.013 | 1.00 | 22.40 |
| + ID2= 2 ( 0102): | 0.01 | 0.001 | 1.17 | 23.05 |
| =====             |      |       |      |       |
| ID = 3 ( 0007):   | 0.14 | 0.014 | 1.00 | 22.45 |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
-----

FINISH

=====

=====

|           |   |   |       |       |   |       |       |    |
|-----------|---|---|-------|-------|---|-------|-------|----|
| V         | V | I | SSSSS | U     | U | A     | L     | (v |
| 6.2.2017) |   |   |       |       |   |       |       |    |
| V         | V | I | SS    | U     | U | A A   | L     |    |
| V         | V | I | SS    | U     | U | AAAAA | L     |    |
| V         | V | I | SS    | U     | U | A A   | L     |    |
| VV        |   | I | SSSSS | UUUUU |   | A A   | LLLLL |    |

|     |       |       |   |   |     |   |    |    |     |    |
|-----|-------|-------|---|---|-----|---|----|----|-----|----|
| OOO | TTTTT | TTTTT | H | H | Y   | Y | M  | M  | OOO | TM |
| O O | T     | T     | H | H | Y Y |   | MM | MM | O O |    |
| O O | T     | T     | H | H | Y   |   | M  | M  | O O |    |
| OOO | T     | T     | H | H | Y   |   | M  | M  | OOO |    |

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2  
\voin.dat

Output filename: C:\Users\kristine.campbell\AppData\Local  
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\8ccd18a5-  
f5dc-4e2b-8067-849f9fd

Summary filename: C:\Users\kristine.campbell\AppData\Local  
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\8ccd18a5-  
f5dc-4e2b-8067-849f9fd

DATE: 08/14/2025

TIME: 02:48:40

USER:

COMMENTS:

```

-----
*****
** SIMULATION : 5yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      | IDF curve parameters: A= 535.364
| Ptotal= 42.59 mm  | B= 0.000
----- C= 0.699
used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs
Storm time step   = 5.00 min
Time to peak ratio = 0.33

```

| TIME | RAIN  | TIME | RAIN   | TIME | RAIN  | TIME | RAIN  |
|------|-------|------|--------|------|-------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr | hrs  | mm/hr |
| 0.00 | 4.59  | 0.75 | 16.12  | 1.50 | 9.96  |      |       |
| 2.25 | 5.64  | 0.83 | 29.99  | 1.58 | 9.09  |      |       |
| 2.33 | 5.40  | 0.92 | 173.81 | 1.67 | 8.38  |      |       |
| 2.42 | 5.19  | 1.00 | 36.80  | 1.75 | 7.80  |      |       |
| 2.50 | 5.00  | 1.08 | 23.21  | 1.83 | 7.30  |      |       |
| 2.58 | 4.83  | 1.17 | 17.70  | 1.92 | 6.88  |      |       |
| 2.67 | 4.67  | 1.25 | 14.58  | 2.00 | 6.51  |      |       |
| 2.75 | 4.52  | 1.33 | 12.53  | 2.08 | 6.18  |      |       |
| 2.83 | 4.38  | 1.42 | 11.07  | 2.17 | 5.89  |      |       |
| 2.92 | 4.25  |      |        |      |       |      |       |

```

-----
-----
| CALIB              |
| NASHYD ( 0102) | Area (ha)= 0.01 Curve Number
(CN)= 74.3
| ID= 1 DT=10.0 min | Ia (mm)= 4.96 # of Linear
Res. (N)= 3.00
----- U.H. Tp(hrs)= 0.17

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

| ----- TRANSFORMED HYETOGRAPH ----- |       |       |       |  |       |        |  |
|------------------------------------|-------|-------|-------|--|-------|--------|--|
| TIME                               | RAIN  | TIME  | RAIN  |  | TIME  | RAIN   |  |
| hrs                                | mm/hr | hrs   | mm/hr |  | hrs   | mm/hr  |  |
| 2.67                               | 4.92  | 0.167 | 4.75  |  | 1.000 | 101.90 |  |
| 2.83                               | 4.59  | 0.333 | 5.53  |  | 1.167 | 30.01  |  |
| 3.00                               | 4.32  | 0.500 | 6.71  |  | 1.333 | 16.14  |  |
|                                    |       | 0.667 | 8.80  |  | 1.500 | 11.80  |  |
|                                    |       | 0.833 | 13.96 |  | 1.667 | 9.52   |  |
|                                    |       |       |       |  | 2.000 | 7.09   |  |
|                                    |       |       |       |  | 2.167 | 6.34   |  |
|                                    |       |       |       |  | 2.333 | 5.76   |  |
|                                    |       |       |       |  | 2.500 | 5.30   |  |

Unit Hyd Qpeak (cms)= 0.003

PEAK FLOW (cms)= 0.000 (i)

TIME TO PEAK (hrs)= 1.167

RUNOFF VOLUME (mm)= 10.653

TOTAL RAINFALL (mm)= 42.586

RUNOFF COEFFICIENT = 0.250

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
-----
| CALIB |
| NASHYD ( 0101) | Area (ha)= 0.13 Curve Number
(CN)= 76.5
| ID= 1 DT=10.0 min | Ia (mm)= 4.68 # of Linear
Res. (N)= 3.00
----- U.H. Tp(hrs)= 0.12

```

NOTE: RAINFALL WAS TRANSFORMED TO 10.0 MIN. TIME STEP.

| ----- TRANSFORMED HYETOGRAPH ----- |       |       |       |  |       |        |  |
|------------------------------------|-------|-------|-------|--|-------|--------|--|
| TIME                               | RAIN  | TIME  | RAIN  |  | TIME  | RAIN   |  |
| hrs                                | mm/hr | hrs   | mm/hr |  | hrs   | mm/hr  |  |
| 2.67                               | 4.92  | 0.167 | 4.75  |  | 1.000 | 101.90 |  |
| 2.83                               | 4.59  | 0.333 | 5.53  |  | 1.167 | 30.01  |  |
| 3.00                               | 4.32  | 0.500 | 6.71  |  | 1.333 | 16.14  |  |
|                                    |       |       |       |  | 2.167 | 6.34   |  |

|       |       |  |       |       |  |       |      |  |
|-------|-------|--|-------|-------|--|-------|------|--|
| 0.667 | 8.80  |  | 1.500 | 11.80 |  | 2.333 | 5.76 |  |
| 0.833 | 13.96 |  | 1.667 | 9.52  |  | 2.500 | 5.30 |  |

Unit Hyd Qpeak (cms)= 0.042

PEAK FLOW (cms)= 0.005 (i)  
 TIME TO PEAK (hrs)= 1.000  
 RUNOFF VOLUME (mm)= 10.634  
 TOTAL RAINFALL (mm)= 42.586  
 RUNOFF COEFFICIENT = 0.250

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

|       |            |      |       |       |
|-------|------------|------|-------|-------|
| ----- |            |      |       |       |
|       | ADD HYD    | (    | 0007) |       |
|       | 1 + 2 =    | 3    |       |       |
| ----- |            |      |       |       |
|       |            | AREA | QPEAK | TPEAK |
|       |            | (ha) | (cms) | (hrs) |
|       |            |      |       | R.V.  |
|       |            |      |       | (mm)  |
|       | ID1= 1 (   | 0.13 | 0.005 | 1.00  |
|       | 0101):     |      |       | 10.63 |
|       | + ID2= 2 ( | 0.01 | 0.000 | 1.17  |
|       | 0102):     |      |       | 10.65 |
| ===== |            |      |       |       |
|       | ID = 3 (   | 0.14 | 0.006 | 1.00  |
|       | 0007):     |      |       | 10.64 |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

```
=====
=====
```

```

      V      V      I      SSSSS      U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V      V      I      SS      U      U      AAAAA      L
      V      V      I      SS      U      U      A      A      L
      VV      I      SSSSS      UUUUU      A      A      LLLLL

```

```

      OOO      TTTTT      TTTTT      H      H      Y      Y      M      M      OOO      TM
      O      O      T      T      H      H      Y      Y      MM      MM      O      O
      O      O      T      T      H      H      Y      M      M      O      O
      OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

```

Input   filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2
\voindat
Output  filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\5c913353-31b0-4e9a-ae8c-28eb8c2
Summary filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\5c913353-31b0-4e9a-ae8c-28eb8c2

```

DATE: 08/14/2025

TIME: 02:55:23

USER:

COMMENTS:

```
-----
-----
```

```

*****
** SIMULATION : 100yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      |      IDF curve parameters: A= 892.273
| Ptotal= 70.98 mm  |      B=    0.000
-----
                                C=    0.699

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN  | TIME | RAIN   | TIME | RAIN  |
|------|-------|------|-------|------|--------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr |
| 0.00 | 7.65  | 0.75 | 26.87 | 1.50 | 16.60  |      |       |
| 2.25 | 9.39  | 0.08 | 8.18  | 0.83 | 49.98  | 1.58 | 15.15 |
| 2.33 | 9.01  | 0.17 | 8.82  | 0.92 | 289.68 | 1.67 | 13.97 |
| 2.42 | 8.66  | 0.25 | 9.60  | 1.00 | 61.34  | 1.75 | 12.99 |
| 2.50 | 8.34  | 0.33 | 10.56 | 1.08 | 38.68  | 1.83 | 12.17 |
| 2.58 | 8.05  | 0.42 | 11.80 | 1.17 | 29.50  | 1.92 | 11.46 |
| 2.67 | 7.78  | 0.50 | 13.47 | 1.25 | 24.30  | 2.00 | 10.84 |
| 2.75 | 7.53  | 0.58 | 15.86 | 1.33 | 20.88  | 2.08 | 10.30 |
| 2.83 | 7.30  | 0.67 | 19.65 | 1.42 | 18.44  | 2.17 | 9.82  |
| 2.92 | 7.09  |      |       |      |        |      |       |

-----

| CALIB             |       | STANDHYD ( 0202) |       | Area (ha)=     | 0.05 |
|-------------------|-------|------------------|-------|----------------|------|
| ID= 1 DT= 5.0 min | 99.90 | Total Imp(%)=    | 99.90 | Dir. Conn.(%)= |      |

|                         | IMPERVIOUS | PERVIOUS (i) |
|-------------------------|------------|--------------|
| Surface Area (ha)=      | 0.05       | 0.00         |
| Dep. Storage (mm)=      | 1.00       | 5.00         |
| Average Slope (%)=      | 8.00       | 2.00         |
| Length (m)=             | 18.26      | 3.00         |
| Mannings n =            | 0.013      | 0.250        |
| Max.Eff.Inten. (mm/hr)= | 289.68     | 66.29        |
| over (min)              | 5.00       | 5.00         |
| Storage Coeff. (min)=   | 0.32 (ii)  | 0.38 (ii)    |
| Unit Hyd. Tpeak (min)=  | 5.00       | 5.00         |
| Unit Hyd. peak (cms)=   | 0.34       | 0.34         |

\*TOTALS\*

|       |                    |        |       |       |
|-------|--------------------|--------|-------|-------|
| 0.040 | PEAK FLOW          | (cms)= | 0.04  | 0.00  |
| 1.00  | TIME TO PEAK       | (hrs)= | 1.00  | 1.00  |
| 69.93 | RUNOFF VOLUME      | (mm)=  | 69.98 | 28.04 |
| 70.98 | TOTAL RAINFALL     | (mm)=  | 70.98 | 70.98 |
| 0.99  | RUNOFF COEFFICIENT | =      | 0.99  | 0.40  |

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
|SOAKAWAY( 0012)| UNDERDRAIN: OFF
|IN= 2--> OUT= 3 |
|DT= 5.0 MIN    | STORAGE LAYER:
-----
(m)= 0.80          Length          (m)= 30.00   Height
                    Porosity        = 0.40     Initial Water
Level              (m)= 0.00
                    Width            (m)= 2.00   Min. Drawdown
(hr)= 24.00
                    Max. Drawdown    (hr)= 62.75   Available
Storage (cu.m.)= 19.20
                    NATIVE SOIL LAYER:
                    Infiltration (m/hr) = 0.0051

```

| R.V.  | AREA           | QPEAK | TPEAK |      |
|-------|----------------|-------|-------|------|
| (mm)  | (ha)           | (cms) | (hrs) |      |
| 69.93 | INFLOW:ID= 2   | 0.05  | 0.040 | 1.00 |
| 29.75 | OVERFLOW:ID= 3 | 0.05  | 0.007 | 1.08 |

Volume Reduction Rate[(RVin-RVout)/RVin] (%):  
If RVout= (Overflow) =

57.46

Time to reach Max storage (Hr)=

1.08

Volume of water for drawdown in LID (cu.m.)=

19.17  
 Volume of maximum water storage (cu.m.)=  
 19.20  
 Calculated Drawdown Time (Hr)=  
 62.58

-----  
 | Junction Command(0013) |  
 -----

|                       | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-----------------------|--------------|----------------|----------------|--------------|
| INFLOW : ID= 3( 0012) | 0.05         | 0.01           | 1.08           | 29.75        |
| OUTFLOW: ID= 2( 0013) | 0.05         | 0.01           | 1.08           | 29.75        |

-----  
 -----

-----  
 | CALIB |  
 | NASHYD ( 0201) | Area (ha)= 0.07 Curve Number  
 (CN)= 74.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.13

Unit Hyd Qpeak (cms)= 0.019

PEAK FLOW (cms)= 0.008 (i)  
 TIME TO PEAK (hrs)= 1.083  
 RUNOFF VOLUME (mm)= 27.759  
 TOTAL RAINFALL (mm)= 70.976  
 RUNOFF COEFFICIENT = 0.391

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

-----  
 | ADD HYD ( 0016) |  
 | 1 + 2 = 3 |  
 -----  

|                   | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-------------------|--------------|----------------|----------------|--------------|
| ID1= 1 ( 0013):   | 0.05         | 0.007          | 1.08           | 29.75        |
| + ID2= 2 ( 0201): | 0.07         | 0.008          | 1.08           | 27.76        |
| =====             |              |                |                |              |
| ID = 3 ( 0016):   | 0.12         | 0.015          | 1.08           | 28.62        |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

-----  
 | CALIB |  
 -----



| STANDHYD ( 0203) | Area (ha)= 0.03  
 | ID= 1 DT= 5.0 min | Total Imp(%)= 56.90 Dir. Conn.(%)= 56.90

```

-----
                        IMPERVIOUS      PERVIOUS (i)
Surface Area      (ha)=      0.02      0.01
Dep. Storage      (mm)=      2.00      5.00
Average Slope      (%)=      2.00      2.00
Length            (m)=     13.90      9.00
Mannings n        =      0.013      0.250

Max.Eff.Inten.(mm/hr)= 289.68      66.29
                        over (min)  5.00      5.00
Storage Coeff. (min)=  0.42 (ii)  2.10 (ii)
Unit Hyd. Tpeak (min)=  5.00      5.00
Unit Hyd. peak  (cms)=  0.34      0.31
  
```

```

*TOTALS*
PEAK FLOW      (cms)=      0.01      0.00
0.017 (iii)
TIME TO PEAK   (hrs)=      1.00      1.00
1.00
RUNOFF VOLUME   (mm)=     68.98      28.04
51.32
TOTAL RAINFALL  (mm)=     70.98      70.98
70.98
RUNOFF COEFFICIENT =      0.97      0.40
0.72
  
```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
     CN\* = 74.0    Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
       THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

```

-----
| ADD HYD ( 0017) |
| 1 + 2 = 3 |
-----
                        AREA      QPEAK      TPEAK      R.V.
                        (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0016):      0.12      0.015      1.08      28.62
+ ID2= 2 ( 0203):      0.03      0.017      1.00      51.32
=====
ID = 3 ( 0017):      0.14      0.023      1.00      33.16
  
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

```
=====
=====
```

```

      V      V      I      SSSSS  U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V V      I      SS      U      U      AAAAA L
      V V      I      SS      U      U      A      A L
      VV      I      SSSSS  UUUUU  A      A  LLLLL

```

```

      OOO      TTTTT  TTTTT  H      H  Y      Y  M      M  OOO      TM
      O      O      T      T      H      H  Y Y      MM MM  O      O
      O      O      T      T      H      H  Y      M      M  O      O
      OOO      T      T      H      H  Y      M      M  OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2  
 \voin.dat  
 Output filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\4f81034c-  
 d9a9-4bc2-ba24-eb656e  
 Summary filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\4f81034c-  
 d9a9-4bc2-ba24-eb656e

DATE: 08/14/2025

TIME: 02:55:23

USER:

COMMENTS:

```
-----
-----
```

```

*****
** SIMULATION : 10yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      |      IDF curve parameters: A= 622.842
| Ptotal= 49.54 mm  |      B=      0.000
-----
|                     |      C=      0.699

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN   | TIME | RAIN  | TIME | RAIN  |
|------|-------|------|--------|------|-------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr | hrs  | mm/hr |
| 0.00 | 5.34  | 0.75 | 18.76  | 1.50 | 11.59 |      |       |
| 2.25 | 6.56  | 0.83 | 34.89  | 1.58 | 10.57 |      |       |
| 2.33 | 6.29  | 0.92 | 202.21 | 1.67 | 9.75  |      |       |
| 2.42 | 6.04  | 1.00 | 42.82  | 1.75 | 9.07  |      |       |
| 2.50 | 5.82  | 1.08 | 27.00  | 1.83 | 8.49  |      |       |
| 2.58 | 5.62  | 1.17 | 20.59  | 1.92 | 8.00  |      |       |
| 2.67 | 5.43  | 1.25 | 16.96  | 2.00 | 7.57  |      |       |
| 2.75 | 5.26  | 1.33 | 14.58  | 2.08 | 7.19  |      |       |
| 2.83 | 5.10  | 1.42 | 12.87  | 2.17 | 6.86  |      |       |
| 2.92 | 4.95  |      |        |      |       |      |       |

-----  
-----

-----  
| CALIB |  
| STANDHYD ( 0202) | Area (ha)= 0.05  
| ID= 1 DT= 5.0 min | Total Imp(%)= 99.90 Dir. Conn.(%)= 99.90  
-----

|                         |       |            |              |
|-------------------------|-------|------------|--------------|
|                         |       | IMPERVIOUS | PERVIOUS (i) |
| Surface Area            | (ha)= | 0.05       | 0.00         |
| Dep. Storage            | (mm)= | 1.00       | 5.00         |
| Average Slope           | (%)=  | 8.00       | 2.00         |
| Length                  | (m)=  | 18.26      | 3.00         |
| Mannings n              | =     | 0.013      | 0.250        |
| Max.Eff.Inten. (mm/hr)= |       | 202.21     | 33.28        |
| over (min)              |       | 5.00       | 5.00         |
| Storage Coeff. (min)=   |       | 0.37 (ii)  | 0.44 (ii)    |
| Unit Hyd. Tpeak (min)=  |       | 5.00       | 5.00         |
| Unit Hyd. peak (cms)=   |       | 0.34       | 0.34         |

\*TOTALS\*

```

    PEAK FLOW      (cms)=      0.03      0.00
0.028 (iii)
    TIME TO PEAK   (hrs)=      1.00      1.00
1.00
    RUNOFF VOLUME   (mm)=      48.54     14.83
48.51
    TOTAL RAINFALL  (mm)=      49.54     49.54
49.54
    RUNOFF COEFFICIENT =      0.98      0.30
0.98

```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
-----
|SOAKAWAY( 0012)| UNDERDRAIN: OFF
|IN= 2--> OUT= 3 |
|DT= 5.0 MIN    | STORAGE LAYER:
-----
(m)= 0.80      Length      (m)= 30.00      Height
Porosity      = 0.40      Initial Water
Level (m)= 0.00      Width      (m)= 2.00      Min. Drawdown
(hr)= 24.00      Max. Drawdown (hr)= 62.75      Available
Storage (cu.m.)= 19.20
NATIVE SOIL LAYER:
Infiltration (m/hr) = 0.0051

```

| R.V.           | AREA | QPEAK | TPEAK |
|----------------|------|-------|-------|
| (mm)           | (ha) | (cms) | (hrs) |
| INFLOW:ID= 2   | 0.05 | 0.028 | 1.00  |
| OVERFLOW:ID= 3 | 0.05 | 0.001 | 1.75  |

```

Volume Reduction Rate[(RVin-RVout)/RVin] (%):
If RVout= (Overflow) =
82.73
Time to reach Max storage (Hr)=
1.67
Volume of water for drawdown in LID (cu.m.)=

```

19.17  
 Volume of maximum water storage (cu.m.)=  
 19.20  
 Calculated Drawdown Time (Hr)=  
 62.58

-----  
 | Junction Command(0013) |  
 -----

|                       | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-----------------------|--------------|----------------|----------------|--------------|
| INFLOW : ID= 3( 0012) | 0.05         | 0.00           | 1.75           | 8.38         |
| OUTFLOW: ID= 2( 0013) | 0.05         | 0.00           | 1.75           | 8.38         |

-----  
 -----

-----  
 | CALIB |  
 | NASHYD ( 0201) | Area (ha)= 0.07 Curve Number  
 (CN)= 74.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.13

Unit Hyd Qpeak (cms)= 0.019

PEAK FLOW (cms)= 0.004 (i)  
 TIME TO PEAK (hrs)= 1.083  
 RUNOFF VOLUME (mm)= 14.680  
 TOTAL RAINFALL (mm)= 49.544  
 RUNOFF COEFFICIENT = 0.296

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

-----  
 | ADD HYD ( 0016) |  
 | 1 + 2 = 3 |  
 -----  

|                   | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-------------------|--------------|----------------|----------------|--------------|
| ID1= 1 ( 0013):   | 0.05         | 0.001          | 1.75           | 8.38         |
| + ID2= 2 ( 0201): | 0.07         | 0.004          | 1.08           | 14.68        |
| =====             |              |                |                |              |
| ID = 3 ( 0016):   | 0.12         | 0.004          | 1.08           | 11.96        |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

-----  
 | CALIB |

```
| STANDHYD ( 0203) | Area (ha)= 0.03
| ID= 1 DT= 5.0 min | Total Imp(%)= 56.90 Dir. Conn.(%)=
56.90
```

```
-----
                        IMPERVIOUS      PERVIOUS (i)
Surface Area (ha)=      0.02          0.01
Dep. Storage (mm)=      2.00          5.00
Average Slope (%)=      2.00          2.00
Length (m)=      13.90          9.00
Mannings n =      0.013          0.250

Max.Eff.Inten.(mm/hr)= 202.21          33.28
over (min)          5.00          5.00
Storage Coeff. (min)= 0.48 (ii)      2.43 (ii)
Unit Hyd. Tpeak (min)= 5.00          5.00
Unit Hyd. peak (cms)= 0.34          0.30
```

\*TOTALS\*

```
PEAK FLOW (cms)=      0.01          0.00
0.011 (iii)
TIME TO PEAK (hrs)=      1.00          1.00
1.00
RUNOFF VOLUME (mm)=      47.54          14.83
33.43
TOTAL RAINFALL (mm)=      49.54          49.54
49.54
RUNOFF COEFFICIENT =      0.96          0.30
0.67
```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
-----
```

```
-----
| ADD HYD ( 0017) |
| 1 + 2 = 3 |
-----
                        AREA      QPEAK      TPEAK      R.V.
                        (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0016):      0.12      0.004      1.08      11.96
+ ID2= 2 ( 0203):      0.03      0.011      1.00      33.43
=====
ID = 3 ( 0017):      0.14      0.014      1.00      16.26
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
-----
```

```
=====
=====
```

```

      V      V      I      SSSSS      U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V      V      I      SS      U      U      AAAAA      L
      V      V      I      SS      U      U      A      A      L
      VV      I      SSSSS      UUUUU      A      A      LLLLL

```

```

      OOO      TTTTT      TTTTT      H      H      Y      Y      M      M      OOO      TM
      O      O      T      T      H      H      Y      Y      MM      MM      O      O
      O      O      T      T      H      H      Y      M      M      O      O
      OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

```

Input   filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2
\voindat
Output  filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\aoce2446-
bf52-4130-8210-f8248c3
Summary filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\aoce2446-
bf52-4130-8210-f8248c3

```

DATE: 08/14/2025

TIME: 02:55:23

USER:

COMMENTS:

```
-----
-----
```

```

*****
** SIMULATION : 25yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      |      IDF curve parameters: A= 731.314
| Ptotal= 58.17 mm  |      B=    0.000
-----                  C=    0.699

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN   | TIME | RAIN  | TIME | RAIN  |
|------|-------|------|--------|------|-------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr | hrs  | mm/hr |
| 0.00 | 6.27  | 0.75 | 22.03  | 1.50 | 13.60 |      |       |
| 2.25 | 7.70  | 0.83 | 40.97  | 1.58 | 12.41 |      |       |
| 2.33 | 7.38  | 0.92 | 237.42 | 1.67 | 11.45 |      |       |
| 2.42 | 7.10  | 1.00 | 50.28  | 1.75 | 10.65 |      |       |
| 2.50 | 6.83  | 1.08 | 31.70  | 1.83 | 9.97  |      |       |
| 2.58 | 6.60  | 1.17 | 24.17  | 1.92 | 9.39  |      |       |
| 2.67 | 6.38  | 1.25 | 19.91  | 2.00 | 8.89  |      |       |
| 2.75 | 6.17  | 1.33 | 17.12  | 2.08 | 8.44  |      |       |
| 2.83 | 5.99  | 1.42 | 15.12  | 2.17 | 8.05  |      |       |
| 2.92 | 5.81  |      |        |      |       |      |       |

-----

|                   |  |                |       |
|-------------------|--|----------------|-------|
| CALIB             |  |                |       |
| STANDHYD ( 0202)  |  | Area (ha)=     | 0.05  |
| ID= 1 DT= 5.0 min |  | Total Imp(%)=  | 99.90 |
| 99.90             |  | Dir. Conn.(%)= |       |

|                         | IMPERVIOUS | PERVIOUS (i) |
|-------------------------|------------|--------------|
| Surface Area (ha)=      | 0.05       | 0.00         |
| Dep. Storage (mm)=      | 1.00       | 5.00         |
| Average Slope (%)=      | 8.00       | 2.00         |
| Length (m)=             | 18.26      | 3.00         |
| Mannings n =            | 0.013      | 0.250        |
| Max.Eff.Inten. (mm/hr)= | 237.42     | 45.68        |
| over (min)              | 5.00       | 5.00         |
| Storage Coeff. (min)=   | 0.35 (ii)  | 0.42 (ii)    |
| Unit Hyd. Tpeak (min)=  | 5.00       | 5.00         |
| Unit Hyd. peak (cms)=   | 0.34       | 0.34         |

\*TOTALS\*



```

    PEAK FLOW      (cms)=      0.03      0.00
0.033 (iii)
    TIME TO PEAK   (hrs)=      1.00      1.00
1.00
    RUNOFF VOLUME  (mm)=      57.17      19.85
57.14
    TOTAL RAINFALL (mm)=      58.17      58.17
58.17
    RUNOFF COEFFICIENT =      0.98      0.34
0.98

```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
-----
|SOAKAWAY( 0012)| UNDERDRAIN: OFF
|IN= 2--> OUT= 3 |
|DT= 5.0 MIN    | STORAGE LAYER:
-----
(m)= 0.80          Length      (m)= 30.00   Height
                    Porosity    = 0.40     Initial Water
Level      (m)= 0.00          Width      (m)= 2.00   Min. Drawdown
(hr)= 24.00          Max. Drawdown (hr)= 62.75   Available
Storage     (cu.m.)= 19.20
                    NATIVE SOIL LAYER:
                    Infiltration (m/hr) = 0.0051

```

| R.V.           | AREA | QPEAK | TPEAK |
|----------------|------|-------|-------|
| (mm)           | (ha) | (cms) | (hrs) |
| INFLOW:ID= 2   | 0.05 | 0.033 | 1.00  |
| OVERFLOW:ID= 3 | 0.05 | 0.003 | 1.33  |

```

Volume Reduction Rate[(RVin-RVout)/RVin] (%):
    If RVout= (Overflow) =
70.33
Time to reach Max storage      (Hr)=
1.25
Volume of water for drawdown in LID (cu.m.)=

```

19.17  
 Volume of maximum water storage (cu.m.)=  
 19.20  
 Calculated Drawdown Time (Hr)=  
 62.58

-----  
 | Junction Command(0013) |  
 -----

|                       | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-----------------------|--------------|----------------|----------------|--------------|
| INFLOW : ID= 3( 0012) | 0.05         | 0.00           | 1.33           | 16.95        |
| OUTFLOW: ID= 2( 0013) | 0.05         | 0.00           | 1.33           | 16.95        |

-----  
 -----

-----  
 | CALIB |  
 | NASHYD ( 0201) | Area (ha)= 0.07 Curve Number  
 (CN)= 74.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.13

Unit Hyd Qpeak (cms)= 0.019

PEAK FLOW (cms)= 0.006 (i)  
 TIME TO PEAK (hrs)= 1.083  
 RUNOFF VOLUME (mm)= 19.651  
 TOTAL RAINFALL (mm)= 58.173  
 RUNOFF COEFFICIENT = 0.338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

-----  
 | ADD HYD ( 0016) |  
 | 1 + 2 = 3 |  
 -----

|                   | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-------------------|--------------|----------------|----------------|--------------|
| ID1= 1 ( 0013):   | 0.05         | 0.003          | 1.33           | 16.95        |
| + ID2= 2 ( 0201): | 0.07         | 0.006          | 1.08           | 19.65        |
| =====             |              |                |                |              |
| ID = 3 ( 0016):   | 0.12         | 0.006          | 1.08           | 18.49        |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

-----  
 | CALIB |  
 -----

```
| STANDHYD ( 0203) | Area (ha)= 0.03
| ID= 1 DT= 5.0 min | Total Imp(%)= 56.90 Dir. Conn.(%)=
56.90
```

```
-----
                        IMPERVIOUS      PERVIOUS (i)
Surface Area (ha)=      0.02          0.01
Dep. Storage (mm)=      2.00          5.00
Average Slope (%)=      2.00          2.00
Length (m)=      13.90          9.00
Mannings n =      0.013          0.250

Max.Eff.Inten.(mm/hr)= 237.42          45.68
over (min)          5.00          5.00
Storage Coeff. (min)= 0.45 (ii)      2.28 (ii)
Unit Hyd. Tpeak (min)= 5.00          5.00
Unit Hyd. peak (cms)= 0.34          0.30
```

\*TOTALS\*

```
PEAK FLOW (cms)=      0.01          0.00
0.013 (iii)
TIME TO PEAK (hrs)=      1.00          1.00
1.00
RUNOFF VOLUME (mm)=      56.17          19.85
40.50
TOTAL RAINFALL (mm)=      58.17          58.17
58.17
RUNOFF COEFFICIENT =      0.97          0.34
0.70
```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
-----
```

```
-----
| ADD HYD ( 0017) |
| 1 + 2 = 3 |
-----
                        AREA      QPEAK      TPEAK      R.V.
                        (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0016):      0.12      0.006      1.08      18.49
+ ID2= 2 ( 0203):      0.03      0.013      1.00      40.50
=====
ID = 3 ( 0017):      0.14      0.017      1.00      22.89
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
-----
```

```
=====
=====
```

```

      V      V      I      SSSSS      U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V      V      I      SS      U      U      AAAAA      L
      V      V      I      SS      U      U      A      A      L
      VV      I      SSSSS      UUUUU      A      A      LLLLL

```

```

      OOO      TTTTT      TTTTT      H      H      Y      Y      M      M      OOO      TM
      O      O      T      T      H      H      Y      Y      MM      MM      O      O
      O      O      T      T      H      H      Y      M      M      O      O
      OOO      T      T      H      H      Y      M      M      OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

```

Input   filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2
\voindat
Output  filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\09105d79-2797-4e99-92ce-8e83521
Summary filename: C:\Users\kristine.campbell\AppData\Local
\Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a
\09105d79-2797-4e99-92ce-8e83521

```

DATE: 08/14/2025

TIME: 02:55:23

USER:

COMMENTS:

```
-----
-----
```

```

*****
** SIMULATION : 50yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      |      IDF curve parameters: A= 813.543
| Ptotal= 64.71 mm  |      B=    0.000
-----
                                C=    0.699

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN   | TIME | RAIN  | TIME | RAIN  |
|------|-------|------|--------|------|-------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr | hrs  | mm/hr |
| 0.00 | 6.97  | 0.75 | 24.50  | 1.50 | 15.13 |      |       |
| 2.25 | 8.56  | 0.83 | 45.57  | 1.58 | 13.81 |      |       |
| 2.33 | 8.21  | 0.92 | 264.12 | 1.67 | 12.74 |      |       |
| 2.42 | 7.89  | 1.00 | 55.93  | 1.75 | 11.85 |      |       |
| 2.50 | 7.60  | 1.08 | 35.26  | 1.83 | 11.09 |      |       |
| 2.58 | 7.34  | 1.17 | 26.89  | 1.92 | 10.45 |      |       |
| 2.67 | 7.09  | 1.25 | 22.15  | 2.00 | 9.89  |      |       |
| 2.75 | 6.87  | 1.33 | 19.04  | 2.08 | 9.39  |      |       |
| 2.83 | 6.66  | 1.42 | 16.82  | 2.17 | 8.96  |      |       |
| 2.92 | 6.47  |      |        |      |       |      |       |

-----

|                   |  |               |                      |
|-------------------|--|---------------|----------------------|
| CALIB             |  |               |                      |
| STANDHYD ( 0202)  |  | Area (ha)=    | 0.05                 |
| ID= 1 DT= 5.0 min |  | Total Imp(%)= | 99.90 Dir. Conn.(%)= |
| 99.90             |  |               |                      |

|                         |       | IMPERVIOUS | PERVIOUS (i) |
|-------------------------|-------|------------|--------------|
| Surface Area            | (ha)= | 0.05       | 0.00         |
| Dep. Storage            | (mm)= | 1.00       | 5.00         |
| Average Slope           | (%)=  | 8.00       | 2.00         |
| Length                  | (m)=  | 18.26      | 3.00         |
| Mannings n              | =     | 0.013      | 0.250        |
| Max.Eff.Inten. (mm/hr)= |       | 264.12     | 55.91        |
| over (min)              |       | 5.00       | 5.00         |
| Storage Coeff. (min)=   |       | 0.33 (ii)  | 0.40 (ii)    |
| Unit Hyd. Tpeak (min)=  |       | 5.00       | 5.00         |
| Unit Hyd. peak (cms)=   |       | 0.34       | 0.34         |

\*TOTALS\*

```

    PEAK FLOW      (cms)=      0.04      0.00
0.037 (iii)
    TIME TO PEAK   (hrs)=      1.00      1.00
1.00
    RUNOFF VOLUME  (mm)=      63.71      23.94
63.67
    TOTAL RAINFALL (mm)=      64.71      64.71
64.71
    RUNOFF COEFFICIENT =      0.98      0.37
0.98

```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
-----
-----
|SOAKAWAY( 0012)| UNDERDRAIN: OFF
|IN= 2--> OUT= 3 |
|DT= 5.0 MIN    | STORAGE LAYER:
-----
(m)= 0.80          Length      (m)= 30.00   Height
                    Porosity    = 0.40     Initial Water
Level      (m)= 0.00          Width      (m)= 2.00   Min. Drawdown
(hr)= 24.00          Max. Drawdown (hr)= 62.75   Available
Storage     (cu.m.)= 19.20
                    NATIVE SOIL LAYER:
                    Infiltration (m/hr) = 0.0051

```

| R.V.           | AREA | QPEAK | TPEAK |
|----------------|------|-------|-------|
| (mm)           | (ha) | (cms) | (hrs) |
| INFLOW:ID= 2   | 0.05 | 0.037 | 1.00  |
| OVERFLOW:ID= 3 | 0.05 | 0.005 | 1.17  |

```

    Volume Reduction Rate[(RVin-RVout)/RVin] (%):
    If RVout= (Overflow) =
63.11
    Time to reach Max storage (Hr)=
1.08
    Volume of water for drawdown in LID (cu.m.)=

```

19.17  
 Volume of maximum water storage (cu.m.)=  
 19.20  
 Calculated Drawdown Time (Hr)=  
 62.58

-----  
 | Junction Command(0013) |  
 -----

|                       | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-----------------------|--------------|----------------|----------------|--------------|
| INFLOW : ID= 3( 0012) | 0.05         | 0.00           | 1.17           | 23.49        |
| OUTFLOW: ID= 2( 0013) | 0.05         | 0.00           | 1.17           | 23.49        |

-----  
 -----

-----  
 | CALIB |  
 | NASHYD ( 0201) | Area (ha)= 0.07 Curve Number  
 (CN)= 74.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.13

Unit Hyd Qpeak (cms)= 0.019

PEAK FLOW (cms)= 0.007 (i)  
 TIME TO PEAK (hrs)= 1.083  
 RUNOFF VOLUME (mm)= 23.694  
 TOTAL RAINFALL (mm)= 64.714  
 RUNOFF COEFFICIENT = 0.366

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

-----  
 | ADD HYD ( 0016) |  
 | 1 + 2 = 3 |  
 -----  

|                   | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-------------------|--------------|----------------|----------------|--------------|
| ID1= 1 ( 0013):   | 0.05         | 0.005          | 1.17           | 23.49        |
| + ID2= 2 ( 0201): | 0.07         | 0.007          | 1.08           | 23.69        |
| =====             |              |                |                |              |
| ID = 3 ( 0016):   | 0.12         | 0.011          | 1.17           | 23.61        |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

-----  
 | CALIB |

```
| STANDHYD ( 0203) | Area (ha)= 0.03
| ID= 1 DT= 5.0 min | Total Imp(%)= 56.90 Dir. Conn.(%)=
56.90
```

```
-----
                        IMPERVIOUS      PERVIOUS (i)
Surface Area (ha)=      0.02      0.01
Dep. Storage (mm)=      2.00      5.00
Average Slope (%)=      2.00      2.00
Length (m)=      13.90      9.00
Mannings n =      0.013      0.250

Max.Eff.Inten.(mm/hr)= 264.12      55.91
over (min)      5.00      5.00
Storage Coeff. (min)= 0.43 (ii)      2.18 (ii)
Unit Hyd. Tpeak (min)= 5.00      5.00
Unit Hyd. peak (cms)= 0.34      0.31
```

\*TOTALS\*

```
PEAK FLOW (cms)=      0.01      0.00
0.015 (iii)
TIME TO PEAK (hrs)=      1.00      1.00
1.00
RUNOFF VOLUME (mm)=      62.71      23.94
45.98
TOTAL RAINFALL (mm)=      64.71      64.71
64.71
RUNOFF COEFFICIENT =      0.97      0.37
0.71
```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
-----
```

```
-----
| ADD HYD ( 0017) |
| 1 + 2 = 3 |
-----
                        AREA      QPEAK      TPEAK      R.V.
                        (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0016):      0.12      0.011      1.17      23.61
+ ID2= 2 ( 0203):      0.03      0.015      1.00      45.98
=====
ID = 3 ( 0017):      0.14      0.020      1.00      28.08
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
-----
```



```
=====
=====
```

```

      V      V      I      SSSSS  U      U      A      L      (v
6.2.2017)
      V      V      I      SS      U      U      A A      L
      V V      I      SS      U      U      AAAAA L
      V V      I      SS      U      U      A      A L
      VV      I      SSSSS  UUUUU  A      A  LLLLL

```

```

      OOO      TTTTT  TTTTT  H      H  Y      Y  M      M  OOO      TM
      O      O      T      T      H      H  Y Y      MM MM  O      O
      O      O      T      T      H      H      Y      M      M  O      O
      OOO      T      T      H      H      Y      M      M  OOO

```

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\*\*\*\*\* D E T A I L E D O U T P U T \*\*\*\*\*

Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2\VO2  
 \voin.dat  
 Output filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\3f62f09e-  
 db1d-4903-88ab-69047c5  
 Summary filename: C:\Users\kristine.campbell\AppData\Local  
 \Civica\XH5\6ec45647-ad21-4b76-932e-273312f20f6a\3f62f09e-  
 db1d-4903-88ab-69047c5

DATE: 08/14/2025

TIME: 02:55:23

USER:

COMMENTS:

```
-----
-----
```

```

*****
** SIMULATION : 5yr 3hr 5min Chicago **
*****

```

```

-----
| CHICAGO STORM      |      IDF curve parameters: A= 535.364
| Ptotal= 42.59 mm  |      B=      0.000
-----
|                     |      C=      0.699

```

used in: INTENSITY = A / (t + B)^C

Duration of storm = 3.00 hrs

Storm time step = 5.00 min

Time to peak ratio = 0.33

| TIME | RAIN  | TIME | RAIN   | TIME | RAIN  | TIME | RAIN  |
|------|-------|------|--------|------|-------|------|-------|
| hrs  | mm/hr | hrs  | mm/hr  | hrs  | mm/hr | hrs  | mm/hr |
| 0.00 | 4.59  | 0.75 | 16.12  | 1.50 | 9.96  |      |       |
| 2.25 | 5.64  | 0.83 | 29.99  | 1.58 | 9.09  |      |       |
| 2.33 | 5.40  | 0.92 | 173.81 | 1.67 | 8.38  |      |       |
| 2.42 | 5.19  | 1.00 | 36.80  | 1.75 | 7.80  |      |       |
| 2.50 | 5.00  | 1.08 | 23.21  | 1.83 | 7.30  |      |       |
| 2.58 | 4.83  | 1.17 | 17.70  | 1.92 | 6.88  |      |       |
| 2.67 | 4.67  | 1.25 | 14.58  | 2.00 | 6.51  |      |       |
| 2.75 | 4.52  | 1.33 | 12.53  | 2.08 | 6.18  |      |       |
| 2.83 | 4.38  | 1.42 | 11.07  | 2.17 | 5.89  |      |       |
| 2.92 | 4.25  |      |        |      |       |      |       |

-----

|                   |  |                |       |
|-------------------|--|----------------|-------|
| CALIB             |  |                |       |
| STANDHYD ( 0202)  |  | Area (ha)=     | 0.05  |
| ID= 1 DT= 5.0 min |  | Total Imp(%)=  | 99.90 |
| 99.90             |  | Dir. Conn.(%)= |       |

|                         | IMPERVIOUS | PERVIOUS (i) |
|-------------------------|------------|--------------|
| Surface Area (ha)=      | 0.05       | 0.00         |
| Dep. Storage (mm)=      | 1.00       | 5.00         |
| Average Slope (%)=      | 8.00       | 2.00         |
| Length (m)=             | 18.26      | 3.00         |
| Mannings n =            | 0.013      | 0.250        |
| Max.Eff.Inten. (mm/hr)= | 173.81     | 24.32        |
| over (min)              | 5.00       | 5.00         |
| Storage Coeff. (min)=   | 0.40 (ii)  | 0.47 (ii)    |
| Unit Hyd. Tpeak (min)=  | 5.00       | 5.00         |
| Unit Hyd. peak (cms)=   | 0.34       | 0.34         |

\*TOTALS\*

|       |                    |        |       |       |
|-------|--------------------|--------|-------|-------|
| 0.024 | PEAK FLOW          | (cms)= | 0.02  | 0.00  |
| 1.00  | TIME TO PEAK       | (hrs)= | 1.00  | 1.00  |
| 41.56 | RUNOFF VOLUME      | (mm)=  | 41.59 | 11.14 |
| 42.59 | TOTAL RAINFALL     | (mm)=  | 42.59 | 42.59 |
| 0.98  | RUNOFF COEFFICIENT | =      | 0.98  | 0.26  |

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
|SOAKAWAY( 0012)| UNDERDRAIN: OFF
|IN= 2--> OUT= 3 |
|DT= 5.0 MIN    | STORAGE LAYER:
-----
(m)= 0.80          Length          (m)= 30.00   Height
                    Porosity       = 0.40     Initial Water
Level              (m)= 0.00
                    Width           (m)= 2.00   Min. Drawdown
(hr)= 24.00
                    Max. Drawdown   (hr)= 62.75   Available
Storage           (cu.m.)= 19.20
                    NATIVE SOIL LAYER:
                    Infiltration (m/hr) = 0.0051

```

| R.V.  | AREA           | QPEAK | TPEAK |      |
|-------|----------------|-------|-------|------|
| (mm)  | (ha)           | (cms) | (hrs) |      |
| 41.56 | INFLOW:ID= 2   | 0.05  | 0.024 | 1.00 |
| 1.42  | OVERFLOW:ID= 3 | 0.05  | 0.001 | 2.75 |

Volume Reduction Rate[(RVin-RVout)/RVin] (%):  
If RVout= (Overflow) =

96.58

Time to reach Max storage (Hr)=

2.67

Volume of water for drawdown in LID (cu.m.)=

19.17  
 Volume of maximum water storage (cu.m.)=  
 19.20  
 Calculated Drawdown Time (Hr)=  
 62.58

-----  
 | Junction Command(0013) |  
 -----

|                       | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-----------------------|--------------|----------------|----------------|--------------|
| INFLOW : ID= 3( 0012) | 0.05         | 0.00           | 2.75           | 1.42         |
| OUTFLOW: ID= 2( 0013) | 0.05         | 0.00           | 2.75           | 1.42         |

-----  
 -----

-----  
 | CALIB |  
 | NASHYD ( 0201) | Area (ha)= 0.07 Curve Number  
 (CN)= 74.0  
 | ID= 1 DT= 5.0 min | Ia (mm)= 5.00 # of Linear  
 Res.(N)= 3.00  
 ----- U.H. Tp(hrs)= 0.13

Unit Hyd Qpeak (cms)= 0.019

PEAK FLOW (cms)= 0.003 (i)  
 TIME TO PEAK (hrs)= 1.083  
 RUNOFF VOLUME (mm)= 11.025  
 TOTAL RAINFALL (mm)= 42.586  
 RUNOFF COEFFICIENT = 0.259

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 -----

-----  
 | ADD HYD ( 0016) |  
 | 1 + 2 = 3 |  
 -----  

|                   | AREA<br>(ha) | QPEAK<br>(cms) | TPEAK<br>(hrs) | R.V.<br>(mm) |
|-------------------|--------------|----------------|----------------|--------------|
| ID1= 1 ( 0013):   | 0.05         | 0.001          | 2.75           | 1.42         |
| + ID2= 2 ( 0201): | 0.07         | 0.003          | 1.08           | 11.02        |
| =====             |              |                |                |              |
| ID = 3 ( 0016):   | 0.12         | 0.003          | 1.08           | 6.89         |

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 -----

-----  
 | CALIB |

```
| STANDHYD ( 0203) | Area (ha)= 0.03
| ID= 1 DT= 5.0 min | Total Imp(%)= 56.90 Dir. Conn.(%)=
56.90
```

```
-----
                        IMPERVIOUS      PERVIOUS (i)
Surface Area (ha)=      0.02      0.01
Dep. Storage (mm)=      2.00      5.00
Average Slope (%)=      2.00      2.00
Length (m)=      13.90      9.00
Mannings n =      0.013      0.250

Max.Eff.Inten.(mm/hr)= 173.81      24.32
over (min)      5.00      5.00
Storage Coeff. (min)= 0.51 (ii)      2.58 (ii)
Unit Hyd. Tpeak (min)= 5.00      5.00
Unit Hyd. peak (cms)= 0.34      0.29
```

```
*TOTALS*
PEAK FLOW (cms)=      0.01      0.00
0.009 (iii)
TIME TO PEAK (hrs)=      1.00      1.00
1.00
RUNOFF VOLUME (mm)=      40.59      11.14
27.88
TOTAL RAINFALL (mm)=      42.59      42.59
42.59
RUNOFF COEFFICIENT =      0.95      0.26
0.65
```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:  
CN\* = 74.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL  
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
-----
```

```
-----
| ADD HYD ( 0017) |
| 1 + 2 = 3 |
-----
                        AREA      QPEAK      TPEAK      R.V.
                        (ha)      (cms)      (hrs)      (mm)
ID1= 1 ( 0016):      0.12      0.003      1.08      6.89
+ ID2= 2 ( 0203):      0.03      0.009      1.00      27.88
=====
ID = 3 ( 0017):      0.14      0.011      1.00      11.08
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
-----
```

FINISH

=====

=====

## **ATTACHMENT C**

### **SANITARY AND WATER DEMAND CALCULATIONS**

---

- Table C.1 – Sanitary Design Flow Calculations
- Table C.2 – Water Design Flow Calculations

Project No: 34397-25  
 Project Name: Proposed Semi Detached Dwellings  
 Project Location: 271 Doyle Street, Southgate  
 Date: 8/15/2025  
 Update: 8/15/2025



**Table C.1: Sanitary Design Flow Calculation**

**Site Characteristics**

|                       |       |        |                                                |
|-----------------------|-------|--------|------------------------------------------------|
| Site Area =           | 0.144 | ha     | *Per Site Plan                                 |
| Number of Units =     | 6     | units  | *Per Site Plan                                 |
| Population per Unit = | 2.938 | ppu    | *Per 2022 Development Charges Background Study |
| Site Population =     | 18    | people |                                                |

**Residential Design Flow**

|                                       |             |            |                                                          |
|---------------------------------------|-------------|------------|----------------------------------------------------------|
| Average Daily Sanitary Flow =         | 350         | L/cap/day  | *Per Southgate Municipal Servicing Standards Section C.1 |
| Site Population =                     | 18          | people     |                                                          |
| Site Average Daily Flow =             | 0.07        | L/s        |                                                          |
| Harmon Peaking Factor =               | 4.00        |            | *Min PF = 2 , Max PF = 4                                 |
| <b>Peak Residential Design Flow =</b> | <b>0.29</b> | <b>L/s</b> | =Average Daily Flow * Peaking Factor                     |

**Inflow and Infiltration**

|                                  |             |            |                                                          |
|----------------------------------|-------------|------------|----------------------------------------------------------|
| Average Inflow per Hectare =     | 0.15        | L/s/ha     | *Per Southgate Municipal Servicing Standards Section C.1 |
| Site Area =                      | 0.144       | ha         |                                                          |
| <b>Total Infiltration Flow =</b> | <b>0.02</b> | <b>L/s</b> |                                                          |

| Design Guideline | Peak Residential Flow<br>(L/s) | Extraneous Flow<br>(L/s) | Peak Design Flow<br>(L/s) |  |
|------------------|--------------------------------|--------------------------|---------------------------|--|
| Southgate        | 0.29                           | 0.02                     | 0.31                      |  |

\*Sanitary design flow calculations completed with reference to the Township of Southgate Municipal Servicing Standards (June 2022)



Project No: 34397-25  
 Project Name: Proposed Semi Detached Dwellings  
 Project Location: 271 Doyle Street, Southgate  
 Date: 8/15/2025  
 Update: 8/15/2025



**Table C.2: Water Design Flow Calculation**

**Site Characteristics**

**Notes:**

|                       |       |        |                                                |
|-----------------------|-------|--------|------------------------------------------------|
| Site Area =           | 0.144 | ha     | *Per Site Plan                                 |
| Number of Units =     | 6     | units  | *Per Site Plan                                 |
| Population per Unit = | 2.938 | ppu    | *Per 2022 Development Charges Background Study |
| Site Population =     | 18    | people |                                                |

**Residential Design Flow**

|                                    |             |            |                                                          |
|------------------------------------|-------------|------------|----------------------------------------------------------|
| Average Daily Water Flow =         | 450         | L/cap/day  | *Per Southgate Municipal Servicing Standards Section E.2 |
| Site Population =                  | 18          | people     |                                                          |
| <b>Site Average Daily Flow =</b>   | <b>0.09</b> | <b>L/s</b> |                                                          |
| MOE Max. Day Peak Factor =         | 9.50        |            | *MOE Design Guidelines, Table 3-3                        |
| MOE Peak Hour Factor =             | 14.30       |            | *MOE Design Guidelines, Table 3-3                        |
| <b>Peak Max. Day Design Flow =</b> | <b>0.89</b> | <b>L/s</b> | =Average Daily Flow * Max Day PF                         |
| <b>Peak Hour Design Flow =</b>     | <b>1.34</b> | <b>L/s</b> | =Average Daily Flow * Max Hour PF                        |

| Design Guideline | Average Daily Flow (L/s) | Max. Day Flow (L/s) | Peak Hour Design Flow (L/s) |
|------------------|--------------------------|---------------------|-----------------------------|
| Southgate/MOE    | 0.09                     | 0.89                | 1.34                        |

\*Water design flow calculations completed with reference to the Township of Southgate Municipal Servicing Standards (June 2022) and the Ministry of Environment Design Guidelines for Drinking-Water Systems (2008)